

## On the Concentrations of Matter Emitted from a Source in the Atmosphere when a 'Flux-Zero' Level Exists above the Source—II (Point source)

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### Introduction

We have reported on the concentrations of matter emitted from a source in the atmosphere when a 'flux-zero' level exists above the source.<sup>(1)</sup> In that paper, in order to elucidate the effects of the 'flux-zero' level on the vertical concentration profiles, consequently on the ground level concentrations, we treated quantitatively only two dimensional cases, namely the phenomena in  $x$  (leeward) and  $z$  (vertical) plane. However, three dimensional phenomena are more important practically, so we investigated numerically the problems for a point source.

### Formulae

We assume that a point source is at  $(0, 0, h)$ , and  $x$ ,  $y$  and  $z$  are coordinates leeward, cross wind and vertically upward respectively. The concentration is given by the eq. 7-31) in the former paper:

$$C = \frac{q}{H} \frac{1}{\pi} \frac{2x}{Au} e^{\frac{2x^2}{A}} \sum_{\nu=0}^{\infty} K_0 \left( \frac{2x}{A} \sqrt{\left(1 + \frac{ABj_\nu^2}{4Hx^2}\right)(x^2 + y^2)} \right) \times \frac{J_0 \left( j_\nu \sqrt{\frac{z}{H}} \right) J_0 \left( j_\nu \sqrt{\frac{h}{H}} \right)}{[J_0(j_\nu)]^2} \quad 1),$$

$$\left. \begin{aligned} A &= q_A(\varphi_A x + e^{-\varphi_A x} - 1) \\ B &= q_B(\varphi_B x + e^{-\varphi_B x} - 1) \end{aligned} \right\} \quad 2),$$

where  $q$  is source intensity (unit/s),  $u$  is wind velocity on the level of the source ( $m/s$ ),  $H$  is the height of the 'flux-zero' level,  $K_0$  is the 1st kind modified Bessel function of the order zero and  $J_0$  is the 1st kind Bessel function of the order zero.  $j$ 's are the zero points of  $J_1$  which is the 1st kind Bessel function of the order 1.  $q_A$ ,  $q_B$ ,  $\varphi_A$  and  $\varphi_B$  are the diffusion parameters<sup>(2)</sup> and they are shown in Table 1.\*

\* In this paper, numerals 4.78 (-2), for example, means  $4.78 \times 10^{-2}$ .

Table 1.  $\varphi_A$ ,  $\sqrt{q_A}$ ,  $\varphi_B$  and  $q_B$ .  $h$  is the source height

$\zeta$	$h$	$\varphi_A$	$\sqrt{q_A}$	$\varphi_B$	$q_B$
0.4	0.5	4.78(-2)	4.26(1)	4.20(-2)	3.50(-1)
	10	4.78(-2)	4.26(1)	4.60(-2)	2.93(-1)
	20	4.78(-2)	4.26(1)	4.71(-2)	2.86(-1)
	30	4.78(-2)	4.26(1)	4.77(-2)	2.83(-1)
	50	4.78(-2)	4.26(1)	4.80(-2)	2.78(-1)
	70	4.78(-2)	4.26(1)	4.81(-2)	2.75(-1)
	100	4.78(-2)	4.26(1)	4.82(-2)	2.70(-1)
	150	4.78(-2)	4.26(1)	4.83(-2)	2.69(-1)
	300	4.78(-2)	4.26(1)	4.84(-2)	2.67(-1)
0	0.5	1.48(-2)	1.56(1)	1.10(-2)	5.30
	10	1.09(-2)	2.18(1)	2.46(-2)	1.02
	20	1.01(-2)	2.37(1)	3.00(-2)	7.00(-1)
	30	9.7(-3)	2.48(1)	3.29(-2)	5.65(-1)
	50	8.2(-3)	2.62(1)	3.79(-2)	4.41(-1)
	70	8.2(-3)	2.71(1)	4.02(-2)	3.80(-1)
	100	8.5(-3)	2.84(1)	4.27(-2)	3.39(-1)
	150	8.3(-3)	2.94(1)	4.40(-2)	3.08(-1)
	300	8.0(-3)	3.04(1)	4.63(-2)	2.93(-1)
-0.1	0.5	4.50(-3)	7.59(1)	4.25(-3)	3.48(1)
	10	2.12(-3)	1.59(2)	1.48(-2)	2.87
	20	1.80(-3)	1.88(2)	1.98(-2)	1.61
	30	1.61(-3)	2.09(2)	2.34(-2)	1.14
	50	1.40(-3)	2.38(2)	2.87(-2)	7.55(-1)
	70	1.29(-3)	2.57(2)	3.30(-2)	5.78(-1)
	100	1.17(-3)	2.85(2)	3.70(-2)	4.59(-1)
	150	1.06(-3)	3.07(2)	4.20(-2)	3.57(-1)
	300	9.8(-4)	3.40(2)	4.44(-2)	3.18(-1)
-0.2	0.5	1.12(-3)	2.77(2)	1.30(-3)	3.73(2)
	10	2.52(-4)	1.24(3)	7.20(-3)	1.18(1)
	20	1.78(-4)	1.73(3)	1.10(-2)	5.19
	30	1.44(-4)	2.14(3)	1.40(-2)	3.21
	50	1.11(-4)	2.77(3)	1.93(-2)	1.69
	70	9.50(-5)	3.30(3)	2.38(-2)	1.11
	100	7.90(-5)	3.93(3)	2.95(-2)	7.22(-1)
	150	6.50(-5)	4.88(3)	3.74(-2)	4.50(-1)
	300	5.60(-5)	5.54(3)	4.28(-2)	3.41(-1)
		4.54(-5)	6.83(3)	4.78(-2)	2.94(-1)

The ground level concentration on the  $x$  axis are given by

$$C_0 = \frac{q}{H} \frac{1}{\pi} \frac{2x}{Au} e^{\frac{2x^2}{4}} \sum_{\nu=0}^{\infty} K_0 \left( \frac{2x^2}{A} \sqrt{1 + \frac{ABj_\nu^2}{4Hx^2}} \right) \frac{J_0 \left( j_\nu \sqrt{\frac{h}{H}} \right)}{J_0(j_\nu)^2} \quad 3).$$

### Numerical calculation

We calculated the ground level concentraions in the cases : stability parameter  $\zeta$  is 0.4 (stable), 0 (neutral),  $-0.2$  (unstable),  $q/u=1$ ,  $h=50, 100, 150, 200, 300, 400$  and  $500 m$  ( $h \leq H$ ).

The shapes of the vertical concentration profiles at every leeward distances are similar to those reported in the former paper, though the absolute values are different because the sources are line in the former paper, but they are point in this paper.

As one example, the profiles in the case  $h=50 m$  and  $\zeta=0$  are shown in Fig. 1.

If we put for ground level concentraions when the height of the 'flux-zero' level is  $H$  as  $C_{H0}$ , and when the level does not exist as  $C_\infty$ , we get the relations between  $C_{H0}$ ,  $C_\infty$  and  $x$  and they are given in Table 2, which are shown graphically in Fig. 2-1-a~2-3-c. In these figures, 1, 2, 3 denote  $h=50, 100, 150 m$  and a, b, c denote  $\zeta=0.4, 0, -0.2$ . Furthermore, the relations between  $C_{H0}/C_\infty$  and  $x$  are given in Table 3.

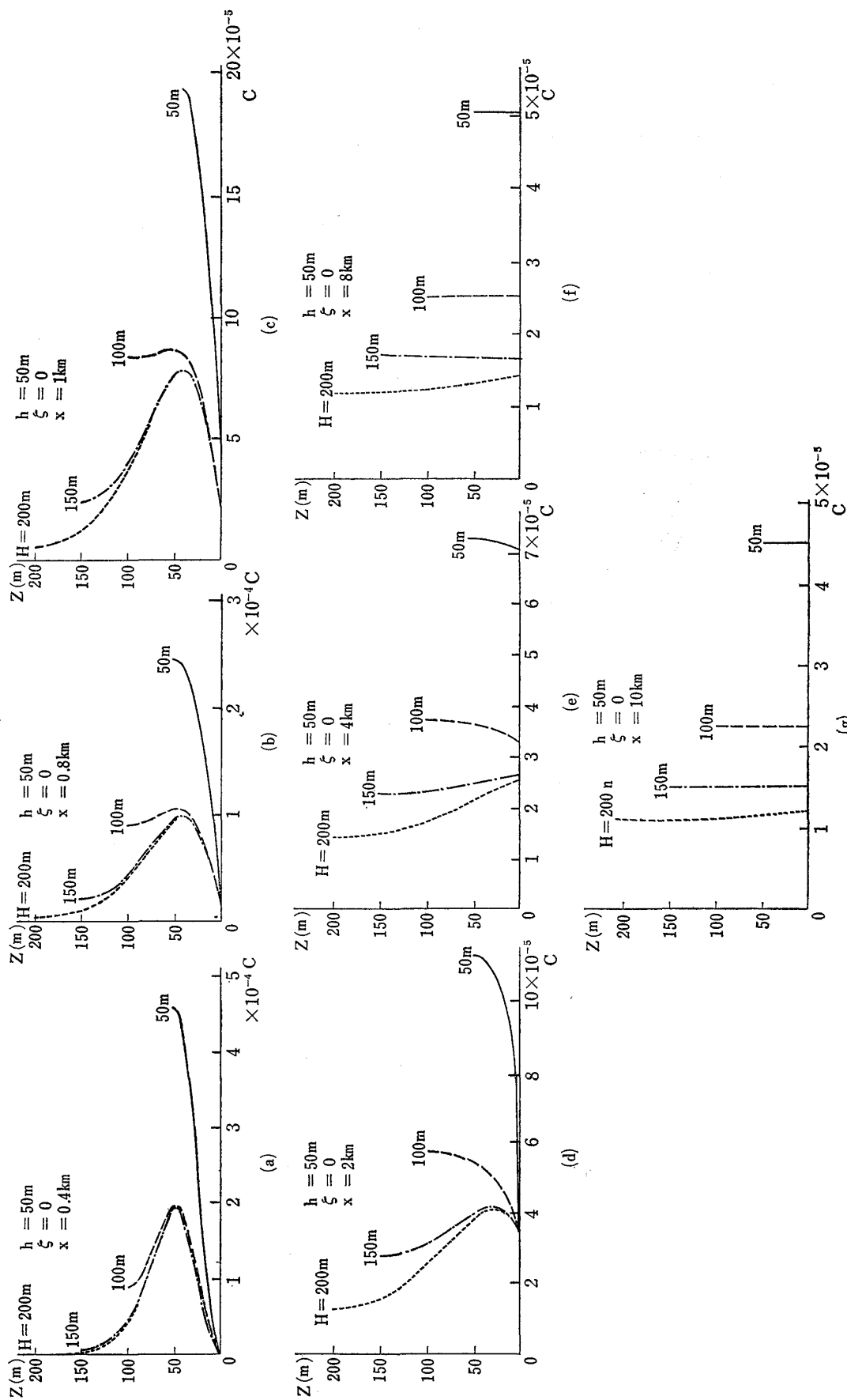


Fig. 1. Concentration profiles for the case of  $h=50\text{m}$ ,  $\xi=0$ .

Table 2. Relations between  $C_{Ho}$ ,  $C_{\infty}$ ,  $H$ ,  $\zeta$  and  $x$ .

		$C_{Ho}$ (h = 50 m)							$C_{\infty}$
$\zeta$	$H$ (H/h)	50 (1)	100 (2)	150 (3)	200 (4)	300 (6)	400 (8)	500 (10)	$\infty$ (0)
0.4	$\frac{x}{h}$	3.748(-10)	1.874(-10)	1.870(-10)	1.862(-10)	1.854(-10)	1.878(-10)	2.451(-10)	1.567(-10)
	200	8.690(-7)	4.230(-7)	4.230(-7)	4.230(-7)	4.230(-7)	4.230(-7)	4.230(-7)	3.143(-7)
	400	3.669(-5)	1.742(-5)	1.742(-5)	1.742(-5)	1.742(-5)	1.742(-5)	1.742(-5)	1.703(-5)
	800	6.942(-5)	3.254(-5)	3.254(-5)	3.254(-5)	3.254(-5)	3.254(-5)	3.254(-5)	3.229(-5)
	1000	1.763(-4)	7.899(-5)	7.769(-5)	7.769(-5)	7.769(-5)	7.769(-5)	7.769(-5)	7.769(-5)
	2000	1.824(-4)	8.339(-5)	7.160(-5)	7.160(-5)	7.160(-5)	7.160(-5)	7.160(-5)	7.058(-5)
	4000	1.356(-4)	6.663(-5)	4.733(-5)	4.733(-5)	3.997(-5)	3.984(-5)	3.984(-5)	3.981(-5)
	8000	1.213(-4)	6.027(-5)	4.145(-5)	3.472(-5)	3.166(-5)	3.133(-5)	3.130(-5)	3.130(-5)
	10000	8.574(-5)	4.318(-5)	2.862(-5)	2.170(-5)	1.590(-5)	1.410(-5)	1.356(-5)	1.333(-5)
20000	6.063(-5)	3.030(-5)	2.021(-5)	1.515(-5)	1.015(-5)	7.794(-6)	5.312(-6)	5.174(-6)	
40000									
0	200	4.481(-8)	2.180(-8)	2.180(-8)	2.180(-8)	2.180(-8)	2.178(-8)	2.200(-8)	2.440(-10)
	400	3.166(-6)	1.519(-6)	1.519(-6)	1.519(-6)	1.519(-6)	1.519(-6)	1.519(-6)	6.975(-7)
	800	3.133(-5)	1.462(-5)	1.461(-5)	1.461(-5)	1.461(-5)	1.461(-5)	1.461(-5)	1.380(-5)
	1000	4.703(-5)	2.166(-5)	2.161(-5)	2.161(-5)	2.161(-5)	2.161(-5)	2.161(-5)	2.137(-5)
	2000	7.984(-5)	3.560(-5)	3.432(-5)	3.432(-5)	3.432(-5)	3.432(-5)	3.432(-5)	3.432(-5)
	4000	7.036(-5)	3.312(-5)	2.656(-5)	2.563(-5)	2.550(-5)	2.549(-5)	2.549(-5)	2.549(-5)
	8000	5.015(-5)	2.505(-5)	1.723(-5)	1.444(-5)	1.316(-5)	1.302(-5)	1.301(-5)	1.301(-5)
	10000	4.506(-5)	2.249(-5)	1.519(-5)	1.215(-5)	1.037(-5)	1.007(-5)	1.003(-5)	1.002(-5)
	20000	3.178(-5)	1.589(-5)	1.060(-5)	7.975(-6)	5.560(-6)	4.654(-6)	4.312(-6)	4.099(-6)
40000	2.245(-5)	1.122(-5)	7.481(-6)	5.612(-6)	3.745(-6)	2.829(-6)	2.313(-6)	1.559(-6)	
-0.2	200	3.436(-6)	1.630(-6)	1.629(-6)	1.629(-6)	1.629(-6)	1.629(-6)	1.629(-6)	8.701(-9)
	400	2.273(-5)	1.047(-5)	1.040(-5)	1.040(-5)	1.040(-5)	1.040(-5)	1.040(-5)	6.900(-6)
	800	4.018(-5)	1.816(-5)	1.723(-5)	1.727(-5)	1.727(-5)	1.727(-5)	1.727(-5)	1.727(-5)
	1000	4.058(-5)	1.836(-5)	1.704(-5)	1.692(-5)	1.690(-5)	1.690(-5)	1.690(-5)	1.690(-5)
	2000	2.710(-5)	1.272(-5)	1.029(-5)	9.799(-6)	9.656(-6)	9.643(-6)	9.643(-6)	9.643(-6)
	4000	1.357(-5)	6.876(-6)	4.856(-6)	4.147(-6)	3.766(-6)	3.693(-6)	3.678(-6)	3.678(-6)
	8000	7.441(-6)	3.645(-6)	2.444(-6)	1.886(-6)	1.434(-6)	1.287(-6)	1.234(-6)	1.189(-6)
	10000	6.030(-6)	3.014(-6)	2.013(-6)	1.530(-6)	1.105(-6)	9.466(-6)	8.817(-7)	8.145(-7)
	20000	3.475(-6)	1.741(-6)	1.161(-6)	8.626(-6)	5.839(-7)	4.472(-7)	3.727(-7)	2.525(-7)
40000	2.171(-6)	1.085(-6)	7.231(-7)	5.427(-7)	3.618(-7)	2.715(-7)	2.175(-7)	8.131(-8)	

a h = 50 m

		$C_{Ho}$ (h = 100 m)						$C_{\infty}$
$\zeta$	$H$ (H/h)	100 (1)	150 (1.5)	200 (2)	300 (3)	400 (4)	500 (5)	$\infty$ (0)
0.4	$\frac{x}{h}$							4.693(-21)
	200							1.001(-11)
	400	2.687(-7)	1.309(-7)	1.309(-7)	1.309(-7)	1.309(-7)	1.309(-7)	1.117(-7)
	800	1.321(-6)	6.396(-7)	6.396(-7)	6.396(-7)	6.396(-7)	6.396(-7)	5.943(-7)
	1000	2.323(-5)	1.115(-5)	1.094(-5)	1.094(-5)	1.094(-5)	1.094(-5)	1.090(-5)
	2000	6.096(-5)	3.131(-5)	2.733(-5)	2.689(-5)	2.689(-5)	2.690(-5)	2.690(-5)
	4000	6.411(-5)	3.863(-5)	2.947(-5)	2.528(-5)	2.496(-5)	2.494(-5)	2.495(-5)
	8000	5.939(-5)	3.733(-5)	2.779(-5)	2.243(-5)	2.172(-5)	2.164(-5)	2.163(-5)
	10000	4.287(-5)	2.850(-5)	2.128(-6)	1.467(-5)	1.236(-5)	1.159(-5)	1.123(-5)
20000	3.030(-5)	2.021(-5)	1.516(-5)	1.027(-5)	7.687(-6)	6.384(-6)	4.808(-6)	
40000								
0	200	3.463(-9)	1.692(-9)	1.692(-9)	1.692(-9)	1.692(-9)	1.692(-9)	2.502(-11)
	400	4.172(-7)	2.017(-7)	2.015(-7)	2.015(-7)	2.015(-7)	2.015(-7)	9.987(-8)
	800	1.275(-6)	6.133(-7)	6.121(-7)	6.121(-7)	6.121(-7)	6.121(-7)	4.319(-7)
	1000	1.149(-5)	5.523(-6)	5.344(-6)	5.388(-6)	5.388(-6)	5.388(-6)	5.238(-6)
	2000	2.421(-5)	1.275(-5)	1.081(-5)	1.052(-5)	1.052(-5)	1.052(-5)	1.052(-5)
	4000	2.324(-5)	1.430(-5)	1.073(-5)	8.978(-6)	8.793(-6)	8.794(-6)	8.794(-6)
	8000	2.128(-5)	1.358(-5)	1.003(-5)	7.881(-6)	7.520(-6)	7.469(-6)	7.470(-6)
	10000	1.520(-5)	1.011(-5)	7.563(-6)	5.160(-6)	4.248(-6)	3.909(-6)	3.720(-6)
	20000	1.073(-5)	7.154(-6)	5.366(-6)	3.578(-6)	2.705(-6)	2.221(-6)	1.560(-6)
40000								
-0.2	200	5.990(-9)	2.905(-9)	2.903(-9)	2.918(-9)	2.677(-9)	1.551(-9)	1.961(-15)
	400	3.300(-7)	1.587(-7)	1.574(-7)	1.574(-7)	1.574(-7)	1.574(-7)	2.233(-9)
	800	2.503(-6)	1.213(-6)	1.167(-6)	1.164(-6)	1.164(-6)	1.164(-6)	4.340(-7)
	1000	3.636(-6)	1.781(-6)	1.681(-6)	1.673(-6)	1.673(-6)	1.673(-6)	9.816(-7)
	2000	6.623(-6)	3.465(-6)	2.997(-6)	2.898(-6)	2.893(-6)	2.893(-6)	2.893(-6)
	4000	5.770(-6)	3.366(-6)	2.637(-6)	2.502(-6)	2.459(-6)	2.453(-6)	2.452(-6)
	8000	3.471(-6)	2.225(-6)	1.664(-6)	1.297(-6)	1.191(-6)	1.161(-6)	1.161(-6)
	10000	2.827(-6)	1.866(-6)	1.393(-6)	1.011(-6)	8.945(-7)	8.556(-7)	8.556(-7)
	20000	1.594(-6)	1.061(-6)	7.951(-7)	5.360(-7)	4.212(-7)	3.651(-7)	3.012(-7)
40000	9.567(-7)	6.378(-7)	4.784(-7)	3.191(-7)	2.400(-7)	1.939(-7)	1.011(-7)	

b h = 100 m

Table 2. Continued.

ζ	H (h/h)	C <sub>Ho</sub> (h = 150 m)					C <sub>∞</sub>
		150 (1)	200 (1.33)	300 (2)	400 (2.7)	500 (3.33)	∞ (0)
0.4	200						
	400						
	800						
	1000	2.392(-9)	1.175(-9)	1.175(-9)	1.175(-9)	1.175(-9)	7.898(-10)
	2000	2.868(-8)	1.403(-8)	1.403(-8)	1.403(-8)	1.403(-8)	1.155(-8)
	4000	3.294(-6)	1.610(-6)	1.579(-6)	1.579(-6)	1.579(-6)	1.552(-6)
	8000	2.222(-5)	1.187(-5)	1.023(-5)	1.022(-5)	1.022(-5)	1.021(-5)
	10000	3.636(-5)	2.317(-5)	1.620(-5)	1.546(-5)	1.540(-5)	1.540(-5)
	20000	3.624(-5)	2.432(-5)	1.627(-5)	1.492(-5)	1.474(-5)	1.472(-5)
40000	2.846(-5)	2.105(-5)	1.375(-5)	1.089(-5)	9.837(-6)	9.269(-6)	
		2.021(-5)	1.516(-5)	1.009(-5)	7.590(-6)	6.199(-6)	4.372(-6)
0	200						
	400						
	800						
	1000	7.063(-9)	3.451(-9)	3.448(-9)	3.451(-9)	3.448(-9)	5.015(-10)
	2000	3.803(-8)	1.855(-8)	1.850(-8)	1.850(-8)	1.850(-8)	6.464(-9)
	4000	1.571(-6)	7.723(-7)	7.493(-7)	7.493(-7)	7.493(-7)	6.718(-7)
	8000	8.487(-6)	4.590(-6)	3.894(-6)	3.881(-6)	3.881(-6)	3.880(-6)
	10000	1.301(-5)	8.375(-6)	5.799(-6)	5.493(-6)	5.480(-6)	5.480(-6)
	20000	1.282(-5)	8.681(-6)	5.778(-6)	5.248(-6)	5.169(-6)	5.167(-6)
40000	9.923(-6)	7.354(-6)	4.812(-6)	3.788(-6)	3.391(-6)	3.170(-6)	
		7.030(-6)	5.272(-6)	3.512(-6)	2.640(-6)	2.150(-6)	1.476(-6)
-0.2	200				1.826(-10)		
	400	7.369(-9)	3.600(-9)	3.560(-9)	5.984(-9)	3.554(-9)	
	800	1.843(-7)	9.175(-8)	8.760(-8)	8.760(-8)	8.760(-8)	
	1000	3.675(-7)	1.853(-7)	1.732(-7)	1.734(-7)	1.734(-7)	2.402(-9)
	2000	1.420(-6)	7.684(-7)	6.548(-7)	6.505(-7)	6.502(-7)	1.635(-8)
	4000	2.395(-6)	1.443(-6)	1.083(-6)	6.505(-7)	6.502(-7)	4.223(-7)
	8000	2.102(-6)	1.424(-6)	1.083(-6)	1.045(-6)	1.040(-6)	1.040(-6)
	10000	1.789(-6)	1.251(-6)	8.314(-7)	8.583(-7)	8.317(-7)	8.317(-7)
	20000	9.932(-7)	7.336(-7)	4.851(-7)	7.149(-7)	6.788(-7)	6.788(-7)
40000	5.869(-7)	4.403(-7)	2.931(-7)	3.781(-7)	3.291(-7)	2.907(-7)	
				2.204(-7)	1.786(-7)	1.062(-7)	

c h=150 m

ζ	H (H/h)	C <sub>Ho</sub> (h = 200 m)				C <sub>∞</sub>
		200 (1)	300 (1.5)	400 (2)	500 (2.5)	∞ (0)
0.4	200					
	400					
	800					
	1000	6.187(-10)	3.042(-10)	3.045(-10)	3.048(-10)	2.097(-10)
	2000	4.590(-7)	2.221(-7)	2.223(-7)	2.223(-7)	2.141(-7)
	4000	8.160(-6)	3.900(-6)	3.883(-6)	3.830(-6)	3.823(-6)
	8000	2.143(-5)	1.101(-5)	9.608(-6)	9.469(-6)	9.461(-6)
	10000	2.330(-5)	1.257(-5)	1.038(-5)	1.003(-5)	9.978(-6)
	20000	2.097(-5)	1.317(-5)	9.805(-6)	8.445(-6)	7.655(-6)
40000	1.515(-5)	1.007(-5)	7.517(-6)	6.054(-6)	3.984(-6)	
0	200					
	400					
	800					
	1000	2.648(-10)	1.298(-10)	1.299(-10)	1.300(-10)	
	2000	2.098(-9)	1.026(-9)	1.026(-9)	1.026(-9)	1.511(-10)
	4000	2.737(-7)	1.321(-7)	1.320(-7)	1.320(-7)	1.036(-7)
	8000	3.294(-6)	1.578(-6)	1.540(-6)	1.539(-6)	1.518(-6)
	10000	7.745(-6)	4.021(-6)	3.466(-6)	3.405(-6)	3.405(-6)
	20000	8.272(-6)	4.515(-6)	3.684(-6)	3.539(-6)	3.521(-6)
40000	7.230(-6)	4.572(-6)	3.400(-6)	2.905(-6)	2.597(-6)	
		5.196(-6)	3.454(-6)	2.582(-6)	2.076(-6)	1.325(-6)
-0.2	200					
	400	1.978(-10)	9.641(-10)	9.593(-10)	1.010(-10)	
	800	1.674(-8)	7.633(-9)	3.982(-9)	7.608(-9)	
	1000	4.251(-8)	2.045(-8)	2.033(-8)	2.032(-8)	1.466(-10)
	2000	3.475(-7)	1.677(-7)	1.862(-7)	1.625(-7)	4.425(-8)
	4000	9.272(-7)	4.651(-7)	4.236(-7)	4.187(-7)	3.660(-7)
	8000	1.239(-6)	6.792(-7)	6.512(-7)	5.320(-7)	5.320(-7)
	10000	1.158(-6)	6.585(-7)	5.256(-7)	4.885(-7)	4.885(-7)
	20000	7.227(-7)	4.566(-7)	3.424(-7)	2.918(-7)	2.631(-7)
40000	4.318(-7)	2.863(-7)	2.139(-7)	1.726(-7)	1.067(-7)	

d h=200 m

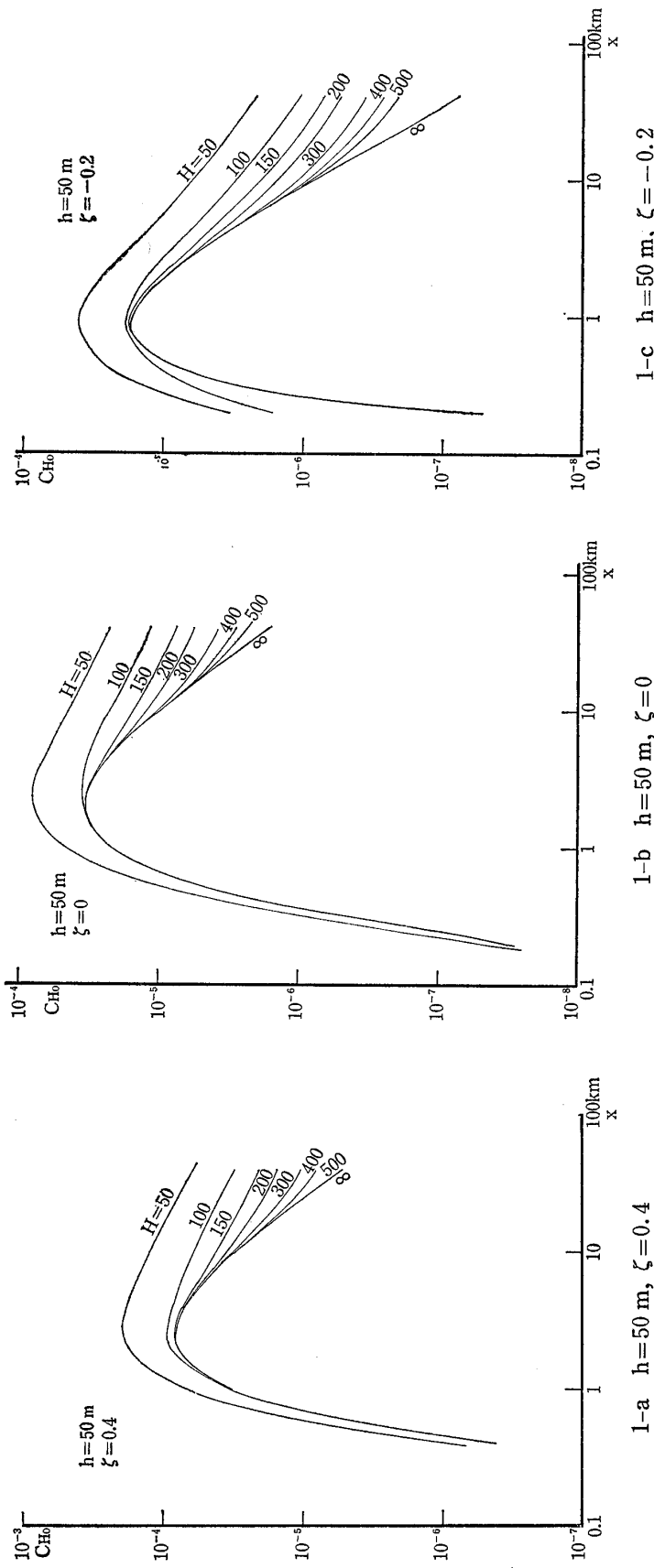
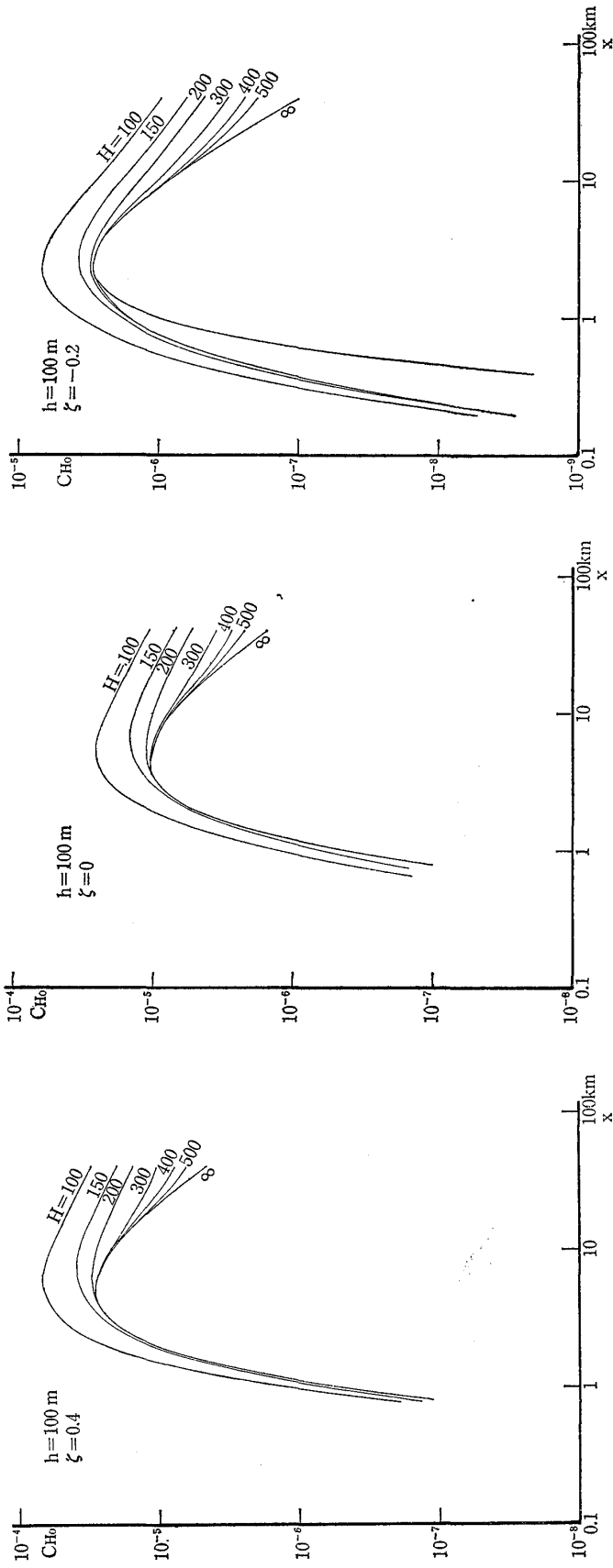


Fig. 2. Relations between  $C_{H_0}$ ,  $H$  and  $x$ .

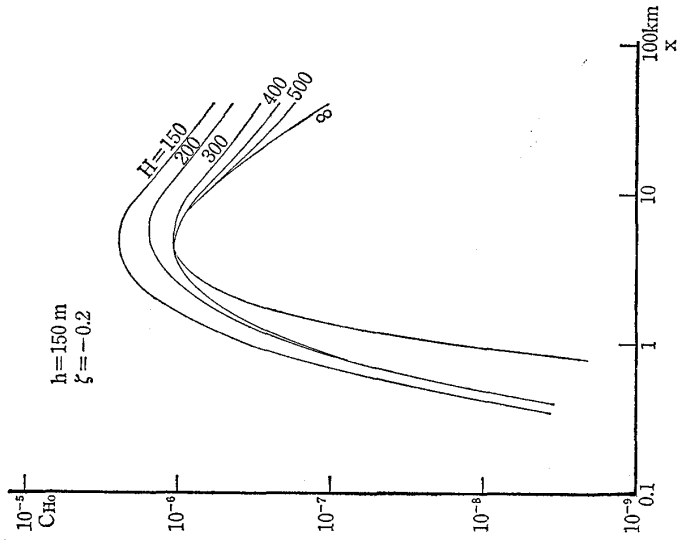


2-a  $h=100$  m,  $\zeta=0.4$

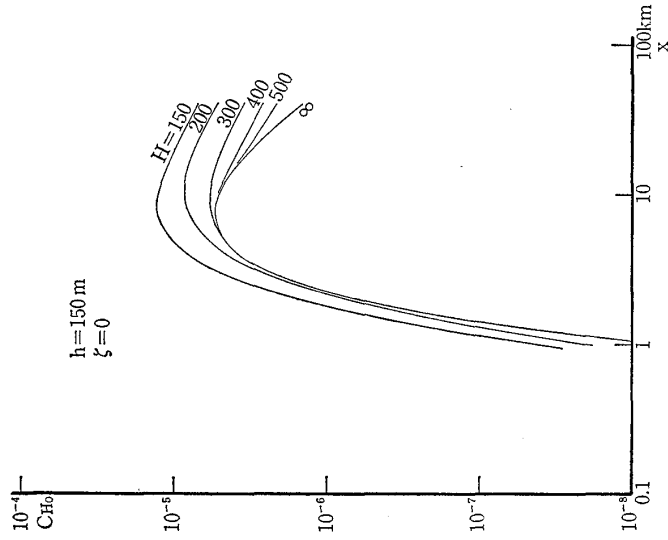
2-b  $h=100$  m,  $\zeta=0$

2-c  $h=100$  m,  $\zeta=-0.2$

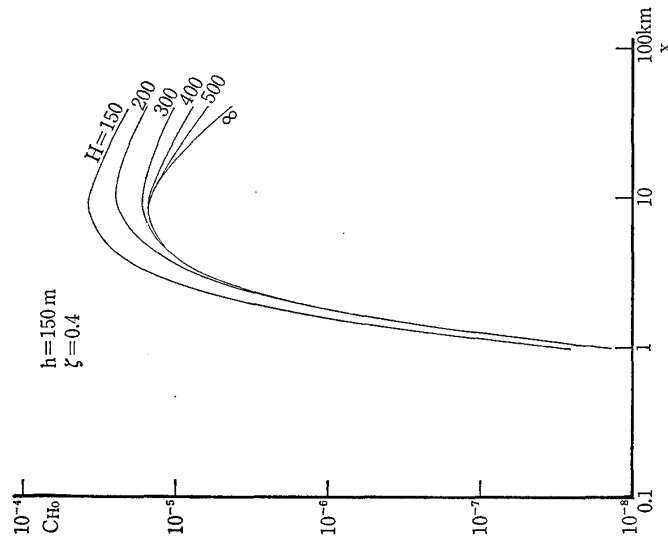
Fig. 2. Continued.



3-c  $h=150$  m,  $\zeta=-0.2$



3-b  $h=150$  m,  $\zeta=0$



3-a  $h=150$  m,  $\zeta=0.4$

Fig. 2. Continued.



Table 3. Relations between  $C_{Ho}/C_{\infty}$ , H,  $\zeta$  and x.

$\zeta$	h (m)										100				
	$\frac{H}{x}$	50								(1)	(1.5)	(2)	(3)	(4)	(5)
		50	100	150	200	300	400	500							
0.4	200														
	400	2.77	1.36	1.36	1.36	1.36	1.36	1.36	1.02	2.41	1.17	1.17	1.17	1.17	1.17
	800	2.15	1.02	1.02	1.02	1.02	1.02	1.02	1.00	2.23	1.08	1.08	1.08	1.08	1.08
	1000	2.15	1.01	1.01	1.01	1.01	1.01	1.01	1.00	2.14	1.02	1.00	1.00	1.00	1.00
	2000	2.27	1.02	1.00	1.00	1.00	1.00	1.00	1.00	2.27	1.17	1.02	1.00	1.00	1.00
	4000	2.58	1.18	1.01	1.00	1.00	1.00	1.00	1.00	2.27	1.17	1.02	1.00	1.00	1.00
	8000	3.40	1.67	1.19	1.05	1.00	1.00	1.00	1.00	2.57	1.55	1.17	1.01	1.00	1.00
	10000	3.88	1.92	1.32	1.15	1.01	1.00	1.00	1.00	2.75	1.73	1.28	1.04	1.00	1.00
	20000	6.43	3.24	2.15	1.62	1.19	1.06	1.02	1.02	3.82	2.54	1.90	1.31	1.10	1.03
	40000	11.7	5.86	3.91	2.93	1.96	1.50	1.02	1.02	6.30	4.21	3.15	2.14	1.60	1.33
0	200														
	400	4.54	2.18	2.18	2.18	2.18	2.18	2.18							
	800	2.27	1.05	1.06	1.06	1.06	1.06	1.06	4.18	2.02	2.02	2.02	2.02	2.02	
	1000	2.20	1.01	1.01	1.01	1.01	1.01	1.01	2.95	1.42	2.42	1.42	1.42	1.42	
	2000	2.33	1.04	1.00	1.00	1.00	1.00	1.00	2.15	1.04	1.00	1.00	1.00	1.00	
	4000	2.76	1.29	1.04	1.00	1.00	1.00	1.00	2.29	1.21	1.02	1.00	1.00	1.00	
	8000	3.88	1.93	1.32	1.11	1.01	1.00	1.00	2.64	1.63	1.22	1.02	1.00	1.00	
	10000	4.50	2.24	1.52	1.21	1.03	1.00	1.00	2.85	1.82	1.34	1.06	1.01	1.00	
	20000		3.88	2.58	1.95	1.36	1.13	1.05	4.09	2.72	2.03	1.39	1.14	1.05	
	40000			4.80	3.60	2.40	1.81	1.48	6.88	4.59	3.44	2.29	1.73	1.42	
-0.2	200														
	400														
	800	2.33	1.05	1.00	1.00	1.00	1.00	1.00	5.77	2.80	2.69	2.68	2.68	2.68	
	1000	2.40	1.09	1.01	1.00	1.00	1.00	1.00	3.70	1.81	1.71	1.70	1.70	1.70	
	2000	2.81	1.32	1.07	1.02	1.00	1.00	1.00	2.29	1.20	1.04	1.00	1.00	1.00	
	4000	3.69	1.81	1.28	1.09	1.00	1.00	1.00	2.35	1.37	1.08	1.02	1.00	1.00	
	8000	6.14	3.07	2.06	1.59	1.21	1.08	1.04	2.99	1.92	1.43	1.03	1.03	1.00	
	10000	7.40	3.70	2.47	1.88	1.36	1.16	1.08	3.30	2.18	1.63	1.18	1.05	1.00	
	20000		6.90	4.60	3.42	2.31	1.77	1.48	5.29	3.52	2.64	1.78	1.40	1.21	
	40000			8.90	6.67	4.45	3.34	2.67		6.31	4.73	3.16	2.37	1.92	

a h=50 and 100 m

$\zeta$	h (m)						200			
	$\frac{H}{x}$	150					(1)	(1.5)	(2)	(2.5)
		150	200	300	400	500				
0.4	200									
	400									
	800	3.05	1.50	1.50	1.50	1.50				
	1000	2.49	1.22	1.22	1.22	1.22	2.95	1.45	1.45	1.45
	2000	2.12	1.04	1.02	1.02	1.02	2.14	1.04	1.04	1.04
	4000	2.18	1.16	1.00	1.00	1.00	2.13	1.02	1.00	1.00
	8000	2.36	1.50	1.05	1.00	1.00	2.27	1.16	1.02	1.00
	10000	2.46	1.65	1.11	1.01	1.00	2.33	1.26	1.04	1.01
	20000	3.07	2.27	1.48	1.18	1.06	2.74	1.72	1.28	1.10
	40000	4.63	3.47	2.31	1.74	1.42	3.80	2.52	1.89	1.52
0	200									
	400									
	800									
	1000	5.88	2.87	2.86	2.86	2.86	2.94	1.45	1.45	1.45
	2000	2.34	1.15	1.12	1.12	1.12	2.14	1.04	1.04	1.04
	4000	2.19	1.18	1.00	1.00	1.00	2.14	1.02	1.00	1.00
	8000	2.37	1.53	1.06	1.00	1.00	2.26	1.16	1.02	1.00
	10000	2.48	1.68	1.12	1.02	1.00	2.34	1.26	1.04	1.01
	20000	3.13	2.32	1.52	1.20	1.07	2.78	1.39	1.36	1.12
	40000	4.76	3.57	2.38	1.79	1.46	3.92	2.61	1.95	1.57
-0.2	200									
	400									
	800									
	1000	2.25	1.13	1.06	1.06	1.06				
	2000	3.36	1.82	1.55	1.54	1.54	7.85	3.79	4.21	3.67
	4000	2.30	1.39	1.04	1.00	1.00	2.53	1.27	1.16	1.14
	8000	2.53	1.71	1.16	1.03	1.00	2.33	1.28	1.22	1.00
	10000	2.64	1.84	1.23	1.05	1.00	2.37	1.35	1.08	1.00
	20000	3.42	2.52	1.67	1.30	1.13	2.75	1.74	1.30	1.11
	40000	5.53	4.15	2.76	2.08	1.68	4.05	2.68	2.01	1.62

b h=150 and 200 m

**Considerations**

The values of  $C_{Ho}/C_{\infty}$  are large when  $x$  is small, and they tend to 1 as  $x$  becomes larger, and then they become larger again when  $x$  becomes much larger. These ratios are larger in unstable conditions

than those in stable conditions. The large ratios near the source are not essential, because the values of  $C_{H_0}$  are originally small.

On the other hand, when  $H/h$  is 1, the values of  $C_{H_0}$  is large, but when  $H/h$  is more than 2, the values are nearly 1, and it shows that the existence of the 'flux-zero' level does not considerably affect the ground level concentration. Furthermore, as it has been remarked in the former paper, the vertical temperature gradient which occurs ordinarily, can not be regarded to be such 'flux-zero' level. We are now carrying out the investigations about the diffusion phenomena in such temperature profiles in the wind tunnel with thermally stratified layers.

### Literature

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