

## On the Concentration of a Plume after when the Wind Direction Changed

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### Introduction

It is not seldom, especially in coastal regions, that the wind which has been blowing in one direction during a certain period, suddenly dies away, and after then it blows again in another direction. A plume which has been emitted from a source in the former stage, drifts with the wind in the second stage. The concentrations of the plume at positions which were to the windward in the former stage are important in the problem of the atmospheric pollution. We consider this problem in the cases when the changes of wind direction are 1)  $180^\circ$ , 2)  $175^\circ$  and 3)  $90^\circ$ .

### Formulation

We assume that the wind has been blowing in the direction  $0\xi$  with the velocity  $u_1$  m/s during  $T$  s, then it changes the direction to  $0x$  and the velocity to  $u_2$  m/s. The relations between coordinates

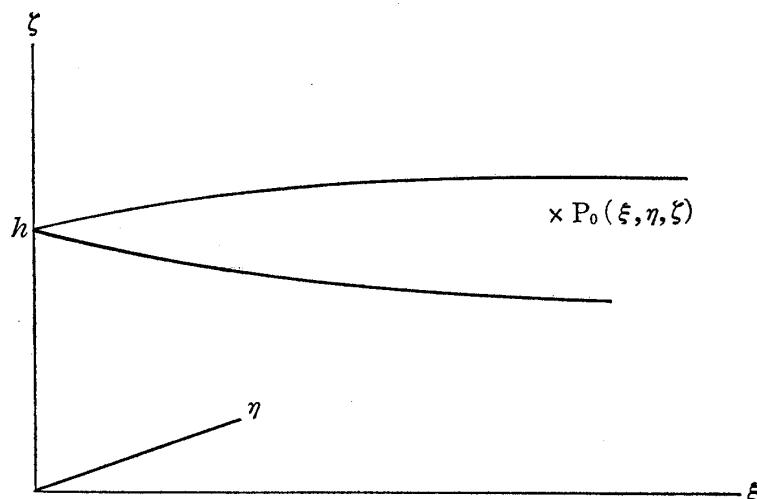
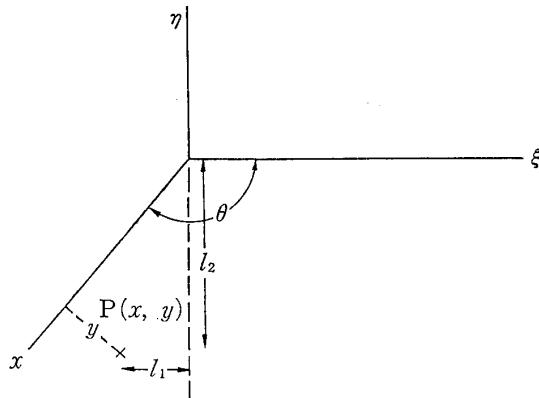


Fig. 1. Coordinates in the 1st stage.

Fig. 2. Relations between  $(\xi, \eta)$  and  $(x, y)$ .

are shown in Figs. 1 and 2. A plume is emitted from a source whose height is  $h$  m above the origin.

The concentration of a puff  $C_1$ , which has been emitted at the instant  $\tau$  ( $0 \leq \tau \leq T$ ) at the point  $P_0(\xi, \eta, \zeta)$  be

$$C_1(\xi, \eta, \zeta, \tau) = q d\tau F_1(\xi, \eta, \zeta, a, b, \tau) \quad 1),$$

where  $q$  is the source intensity of the continuous source, so  $qd\tau$  is that of the instantaneous source.  $a$  and  $b$  are defined by eq. 5 or 7).

The concentration  $C_2$  at the instant  $t$  in the second stage, due to the puff centered at  $P_0$ , is given by

$$C_2(x, y, z, \tau, t) = \int_0^\infty d\zeta \int_{-\infty}^\infty d\eta \int_{-\infty}^\infty C_1(\xi, \eta, \zeta, \tau) F_2(x, y, z, \xi, \eta, \zeta, t) d\xi \quad 2).$$

So the resulted concentration due to the puffs emitted during the whole period  $T$  is given by

$$C_3(x, y, z, t) = \int_0^T d\tau \int_0^\infty d\zeta \int_{-\infty}^\infty d\eta \int_{-\infty}^\infty C_1 F_2 d\xi \quad 3).$$

The functions  $F_1$  and  $F_2$  are given by next two equations :

$$F_1(\xi, \eta, \zeta, \tau) = \frac{e^{-\frac{(\xi-u_1\tau)^2+\eta^2}{a_1}-\frac{h+\zeta}{b_1}}}{a_1 b_1 \pi} I_0\left(\frac{2\sqrt{h}\zeta}{b_1}\right) \quad 4),$$

$$\left. \begin{array}{l} a_1 = q_A (\varphi_A u_1 \tau + e^{-\varphi_A u_1 \tau} - 1) \\ b_1 = q_B (\varphi_B u_1 \tau + e^{-\varphi_B u_1 \tau} - 1) \end{array} \right\} \quad 5).$$

$$F_2(x, y, z, \xi, \eta, \zeta, t) = \frac{1}{a_2 b_2 \pi} e^{-\frac{(x-\xi \cos \theta + \eta \sin \theta - u_2 t)^2}{a_2}} \\ \times e^{-\frac{(\xi \sin \theta + \eta \cos \theta + y)^2}{a_2}} e^{-\frac{\zeta+z}{b_2}} I_0\left(\frac{2\sqrt{\zeta z}}{b_2}\right) \quad 6),$$

$$\left. \begin{array}{l} a_2 = q_A (\varphi_A u_2 t + e^{-\varphi_A u_2 t} - 1) \\ b_2 = q_B (\varphi_B u_2 t + e^{-\varphi_B u_2 t} - 1) \end{array} \right\} \quad 7),$$

where  $q_A, q_B, \varphi_A, \varphi_B$ , are the diffusion parameters which are shown in

Table 1 and  $I_0$  is the 1st kind modified Bessel function of the order 0<sup>(1)\*</sup>.

Table 1.  $\varphi_A$ ,  $\sqrt{q_A}$ ,  $\varphi_B$ ,  $q_B$ ,  $h$  and  $\zeta$ .  $h$  is the source height.

$\zeta$	$h$	$\varphi_A$	$\sqrt{q_A}$	$\varphi_B$	$q_B$
0.4	0.5	4.78(-2)	4.26(1)	4.20(-2)	3.50(-1)
	10	4.78(-2)	4.26(1)	4.60(-2)	2.93(-1)
	20	4.78(-2)	4.26(1)	4.71(-2)	2.86(-1)
	30	4.78(-2)	4.26(1)	4.77(-2)	2.83(-1)
	50	4.78(-2)	4.26(1)	4.80(-2)	2.78(-1)
	70	4.78(-2)	4.26(1)	4.81(-2)	2.75(-1)
	100	4.78(-2)	4.26(1)	4.82(-2)	2.70(-1)
	150	4.78(-2)	4.26(1)	4.83(-2)	2.69(-1)
	200	4.78(-2)	4.26(1)	4.84(-2)	2.67(-1)
	300	4.78(-2)	4.26(1)	4.84(-2)	2.64(-1)
0	0.5	1.48(-2)	1.56(1)	1.10(-2)	5.30
	10	1.09(-2)	2.18(1)	2.46(-2)	1.02
	20	1.01(-2)	2.37(1)	3.08(-2)	9.00(-1)
	30	9.7(-3)	2.48(1)	3.29(-2)	5.55(-1)
	50	9.2(-3)	2.52(1)	3.42(-2)	4.91(-1)
	70	8.6(-3)	2.74(1)	3.02(-2)	3.80(-1)
	100	8.6(-3)	2.88(1)	4.27(-2)	3.39(-1)
	150	8.3(-3)	2.98(1)	4.40(-2)	3.08(-1)
	200	8.0(-3)	3.04(1)	4.63(-2)	2.93(-1)
	300	7.7(-3)	3.23(1)	4.75(-2)	2.78(-1)
-0.1	0.5	4.50(-3)	7.59(1)	4.25(-3)	3.48(1)
	10	2.12(-3)	1.59(2)	1.48(-2)	2.87
	20	1.80(-3)	1.88(2)	1.98(-2)	1.61
	30	1.61(-3)	2.09(2)	2.34(-2)	1.14
	50	1.40(-3)	2.38(2)	2.67(-2)	7.55(-1)
	70	1.29(-3)	2.57(2)	3.10(-2)	5.78(-1)
	100	1.17(-3)	2.67(2)	3.70(-2)	4.59(-1)
	150	1.06(-3)	2.77(2)	4.20(-2)	3.77(-1)
	200	9.8(-4)	3.40(2)	4.44(-2)	3.18(-1)
	300	9.8(-4)	3.66(2)	4.78(-2)	2.79(-1)
-0.2	0.5	1.12(-3)	2.77(2)	1.30(-3)	3.73(2)
	10	2.52(-4)	1.24(3)	7.20(-3)	1.18(1)
	20	1.78(-4)	1.73(3)	1.10(-2)	5.19
	30	1.44(-4)	2.14(3)	1.40(-2)	3.21
	50	1.11(-4)	2.77(3)	1.93(-2)	1.69
	70	9.50(-5)	3.30(3)	2.38(-2)	1.11
	100	7.90(-5)	3.93(3)	2.95(-2)	7.22(-1)
	150	6.50(-5)	4.88(3)	3.74(-2)	4.50(-1)
	200	5.60(-5)	5.54(3)	4.28(-2)	3.41(-1)
	300	4.54(-5)	6.83(3)	4.78(-2)	2.94(-1)

According to the above equations, we get

$$\begin{aligned}
 C_s(x, y, z, t) = & \int_0^T q d\tau \int_0^\infty d\zeta \int_{-\infty}^\infty d\eta \int_{-\infty}^\infty \frac{d\xi}{a_2 a_2 b_1 b_2 \pi} \\
 & \times \exp \left[ - \left\{ \frac{(\xi - u_1 \tau)^2}{a_1} + \frac{\eta^2}{a_1} + \frac{(x - \xi \cos \theta + \eta \sin \theta - u_2 t)^2}{a_2} \right. \right. \\
 & \left. \left. + \frac{(\xi \sin \theta + \eta \cos \theta + y)^2}{a_2} + \frac{h + \zeta}{b_1} + \frac{\zeta + z}{b_2} \right\} \right] I_0 \left( \frac{2\sqrt{h}\zeta}{b_1} \right) I_0 \left( \frac{2\sqrt{\zeta}z}{b_2} \right) \quad 8), \\
 = & \int_0^T \frac{q}{(a_1 + a_2)(b_1 + b_2)\pi} e^{-\frac{1}{a_1 + a_2}[(l_2 - u_2 t \sin \theta)^2]} \\
 & \times e^{-\frac{1}{b_1 + b_2}(u_1 \tau + u_2 t \cos \theta - l_1)^2} e^{-\frac{h+z}{b_1 + b_2}} I_0 \left( \frac{2\sqrt{h}z}{b_1 + b_2} \right) d\tau \quad 9).
 \end{aligned}$$

The ground level concentration is given by

$$\begin{aligned}
 C_s(x, y, 0, t) = & \int_0^T \frac{q}{(a_1 + a_2)(b_1 + b_2)\pi} e^{-\frac{1}{a_1 + a_2}[(l_2 - u_2 t \sin \theta)^2 + (u_1 \tau + u_2 t \cos \theta - l_1)^2]} \\
 & \times e^{-\frac{h}{b_1 + b_2}} d\tau \quad 10).
 \end{aligned}$$

\*) In this paper the numerals 4.78(-2), for example, means  $4.78 \times 10^{-2}$ .

### Approximated calculation

As the parameters  $a_1$  and  $b_1$  are the functions of  $\tau$ , it is very tedious to carry out the integration exactly. So we integrate the eqs. 10) and 11) approximately by putting  $a_{10}$  and  $b_{10}$  instead of  $a_1$  and  $b_1$ , where

$$\tau_0 = \frac{1}{u_1} (l_1 - u_2 t \cos \theta) \quad 11).$$

When  $\tau_0 \geq 0$ ,

$$\left. \begin{aligned} a_{10} &= q_A (\varphi_A u_1 \tau_0 + e^{-\varphi_A u_1 \tau_0} - 1) \\ b_{10} &= q_B (\varphi_B u_1 \tau_0 + e^{-\varphi_B u_1 \tau_0} - 1) \end{aligned} \right\} \quad 12),$$

and when  $\tau_0 < 0$

$$a_{10} = b_{10} = 0 \quad 13).$$

Then we get approximately for eq. 9),

$$\begin{aligned} C_4 = C_4(x, y, z, t) &= \frac{q}{u_1 \sqrt{a_{10} + a_2} (b_{10} + b_2) \sqrt{\pi}} e^{-\frac{1}{a_{10} + a_2} (l_2 - u_2 t \sin \theta)^2} \\ &\times e^{-\frac{h+z}{b_{10} + b_2}} I_0 \left( \frac{2 \sqrt{h} z}{b_{10} + b_2} \right) \frac{1}{2} \left[ \operatorname{erf} \left( \frac{u_1 T + u_2 t \cos \theta - l_1}{\sqrt{a_{10} + a_2}} \right) \right. \\ &\quad \left. - \operatorname{erf} \left( \frac{u_2 t \cos \theta - l_1}{\sqrt{a_{10} + a_2}} \right) \right] \end{aligned} \quad 14),$$

and for eq. 10),

$$\begin{aligned} C_{4,0} = C_4(x, y, 0, t) &= \frac{q}{u_1 \sqrt{a_{10} + a_2} (b_{10} + b_2) \sqrt{\pi}} e^{-\frac{1}{a_{10} + a_2} (l_2 - u_2 t \sin \theta)^2} \\ &\times e^{-\frac{h}{b_{10} + b_2}} \frac{1}{2} \left[ \operatorname{erf} \left( \frac{u_1 T + u_2 t \cos \theta - l_1}{\sqrt{a_{10} + a_2}} \right) - \operatorname{erf} \left( \frac{u_2 t \cos \theta - l_1}{\sqrt{a_{10} + a_2}} \right) \right] \end{aligned} \quad 15).$$

In these equations,  $\operatorname{erf}(\phi)$  is the error integral which is defined by

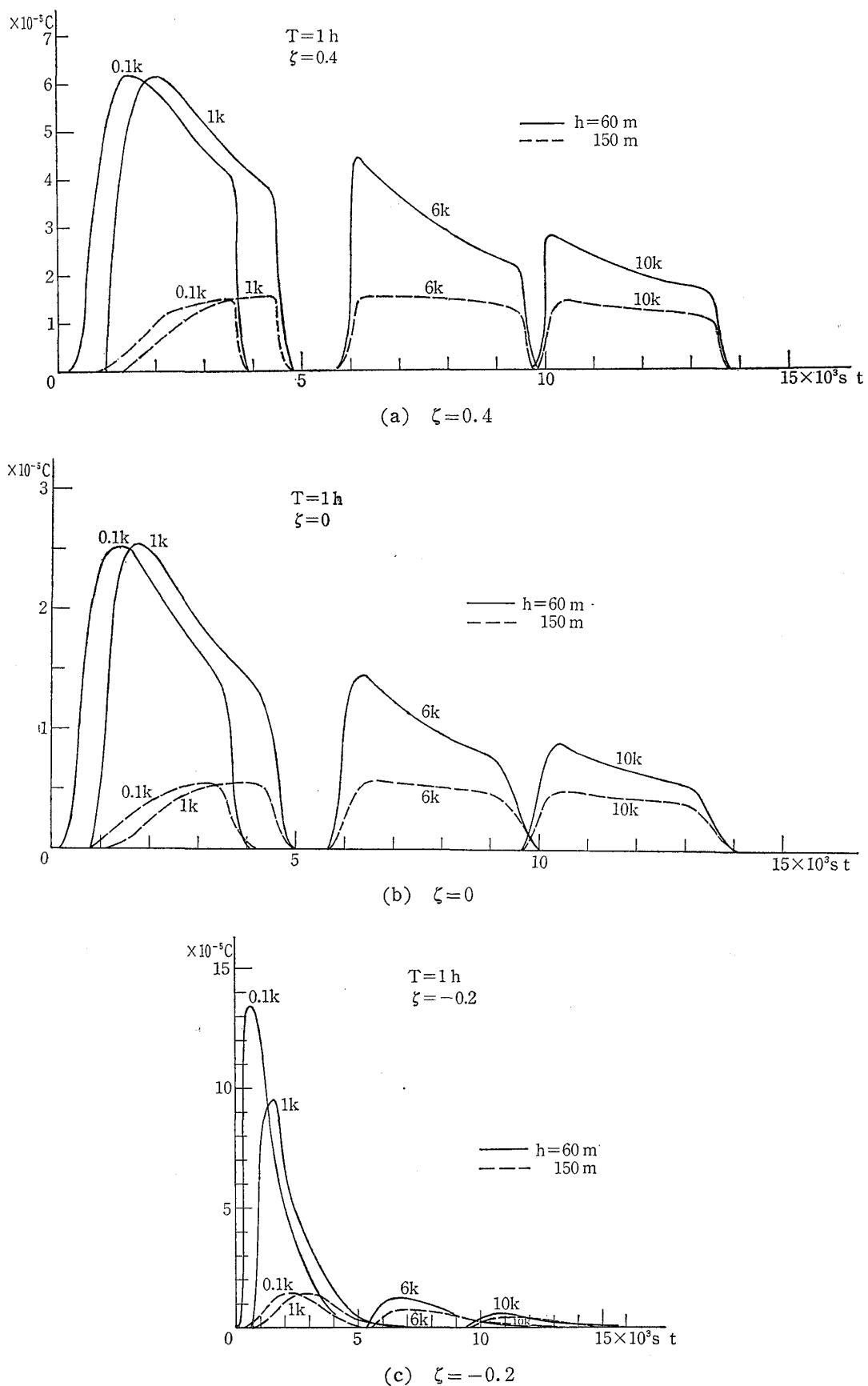
$$\operatorname{erf}(\phi) = \frac{2}{\sqrt{\pi}} \int_0^\phi e^{-u^2} du \quad 16).$$

### Results

1)  $\theta = 180^\circ$ : We calculated the ground level concentrations in the cases of  $h=60, 100, 150$  m,  $T=1, 2, 3$  h, stability parameter  $\zeta=0.4$  (stable), 0 (neutral),  $-0.2$  (unstable),  $q/u_1=1$  and  $u_1=u_2=1$  m/s.

The time changes of concentration are shown in Fig. 3 and 4. Contrary to the concentration in the case of continuous plume, it changes remarkably with time, and it becomes noticeable only during a certain period, exposed interval  $\lambda$ . So, for the air pollution problems, the quantities, dosage  $D$ ,

$$D = \int_0^\infty C dt \text{ c. h} = \frac{1}{3600} \int_0^\infty C dt \text{ c. s}$$

Fig. 3. Time changes of concentration.  $T = 1 \text{ h}$ ,  $h = 60$  and  $150 \text{ m}$ .

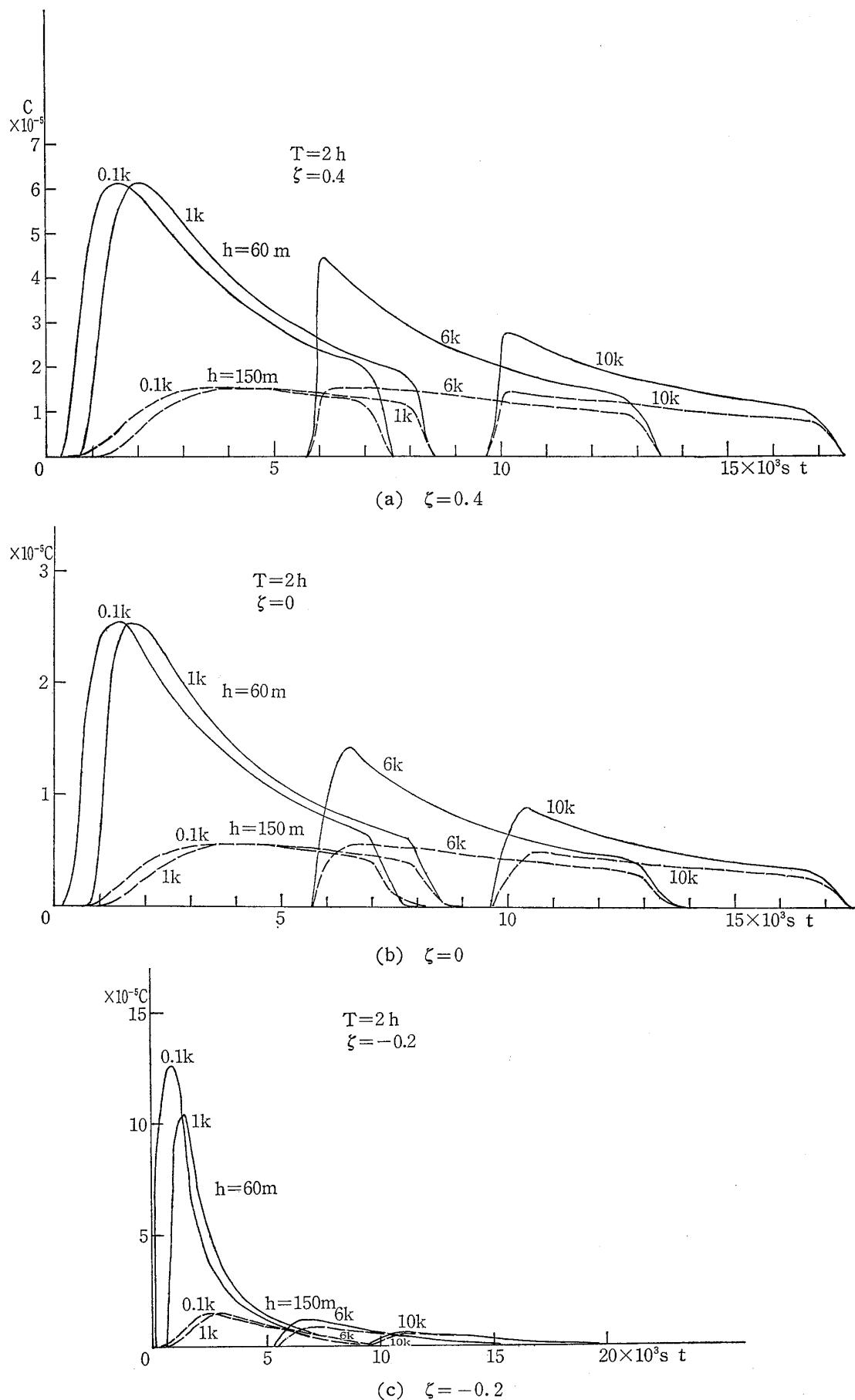


Fig. 4. Time changes of concentration  $T = 2$  h,  $h = 60$  and  $150$  m.

Table 2. Relations between  $C_{\max}$ ,  $D$ ,  $\bar{C}$ ,  $C_e$ ,  $\lambda$  and  $x$ 

$T = 1 \text{ h} (3600 \text{ s}) \quad h = 60 \text{ m}$		$T = 2 \text{ h} (7200 \text{ s}) \quad h = 60 \text{ m}$		$T = 3 \text{ h} (10800 \text{ s}) \quad h = 60 \text{ m}$	
$\zeta$	$x$	$C_{\max}$	$D$	$\bar{C}$	$\lambda$ (s)
	m	$10^{-5}$	$10^{-5}$	$10^{-5}$	$10^{-5}$
$\gamma^* 0$	100	6.154	4.122	3.68	
	200	6.158	4.122	3.72	
	400	4.466	4.07	4.06	0.0041
	600	6.156	4.159	4.24	0.0435
	800	4.484	4.24	4.06	0.0377
	1000	6.155	4.157	4.20	0.07
	2000	6.155	4.159	4.26	0.07
	4000	5.169	3.970	3.42	0.07
	6000	6.159	4.162	4.10	0.0462
	8000	4.497	4.167	4.13	0.0537
$\gamma^* 0$	10000	2.199	2.162	2.16	0.0537
	20000	2.199	2.162	2.16	0.0537
	40000	0.9660	0.9660	0.9659	0.0537
	60000	0.9668	0.9668	0.9668	0.0537
	80000	0.1353	0.1353	0.1353	0.0537
	100000	0.1353	0.1353	0.1353	0.0537
	100	2.545	1.774	1.57	0.06
	200	2.551	1.792	1.56	0.06
	400	2.555	1.829	1.53	0.06
	600	2.555	1.863	1.54	0.06
$\gamma^* 0$	800	2.555	1.889	1.55	0.06
	1000	2.555	1.903	1.55	0.06
	2000	2.524	1.798	1.41	0.07
	4000	1.961	1.382	1.44	0.07
	6000	1.456	1.064	1.08	0.07
	8000	1.113	0.843	0.817	0.07
	10000	0.8775	0.6911	0.517	0.07
	20000	0.3772	0.2308	0.235	0.07
	40000	0.1459	0.1291	0.0916	0.07
	60000	0.0805	0.08029	0.08029	0.07
$\gamma^* 0$	100000	0.0407	0.03896	0.03896	0.07
	100	1.283	0.6103	0.239	8.49
	200	1.258	0.6096	0.236	8.56
	400	1.190	0.6008	0.241	8.99
	600	1.134	0.5808	0.211	9.06
	800	1.042	0.5508	0.211	9.37
	1000	0.953	0.5132	0.194	9.54
	2000	0.567	0.3127	0.110	10.31
	4000	0.2275	0.1744	0.0329	11.66
	6000	0.1213	0.1058	0.0395	12.33
$\gamma^* 0$	8000	0.0732	0.0717	0.0184	13.05
	10000	0.0572	0.0516	0.0123	14.95
	20000	0.0168	0.00346	0.00168	17.51
	40000	0.0039	0.00530	0.00073	23.44
	60000	0.0013	0.00274	0.00032	30.06
	100000	0.0004	0.00121	0.00011	37.08
	100	1.268	0.7189	0.169	15.3
	200	1.269	0.7164	0.168	15.4
	400	1.269	0.7080	0.168	15.5
	600	1.222	0.6806	0.154	16.9
$\gamma^* 0$	800	1.135	0.6166	0.105	16.2
	1000	1.039	0.6066	0.105	16.9
	2000	0.5703	0.4225	0.0477	17.7
	4000	0.2162	0.2347	0.0477	18.59
	6000	0.1171	0.1550	0.0593	18.8
	8000	0.0755	0.1093	0.0199	19.8
	10000	0.0471	0.0871	0.0425	20.5
	20000	0.0168	0.0210	0.0145	20.5
	40000	0.0048	0.0132	0.00139	20.1
	60000	0.0022	0.00619	0.000539	20.3
$\gamma^* 0$	100000	0.0003	0.00268	0.000210	40.4
	100	6.154	4.122	3.68	0.0006
	200	6.158	4.122	3.72	0.00041
	400	4.466	4.07	4.06	0.0435
	600	6.156	4.159	4.24	0.0377
	800	4.484	4.24	4.06	0.07
	1000	6.155	4.157	4.20	0.07
	2000	6.155	4.159	4.26	0.07
	4000	5.169	3.970	3.42	0.0537
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$\gamma^* 0$	8000	4.497	4.167	4.13	0.0537
	10000	2.199	2.162	2.16	0.0537
	20000	2.199	2.162	2.16	0.0537
	40000	0.9660	0.9660	0.9659	0.0537
	60000	0.9668	0.9668	0.9668	0.0537
	80000	0.1353	0.1353	0.1353	0.0537
	100000	0.1353	0.1353	0.1353	0.0537
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	800	2.555	1.889	1.55	0.06
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	2000	2.524	1.798	1.41	0.07
	4000	1.961	1.382	1.44	0.07
	6000	1.456	1.064	1.08	0.07
	8000	1.113	0.843	0.817	0.07
	10000	0.8775	0.6911	0.517	0.07
	20000	0.3772	0.2308	0.235	0.07
	40000	0.1459	0.1291	0.0916	0.07
$\gamma^* 0$	60000	0.0805	0.08029	0.08029	0.07
	80000	0.0407	0.03896	0.03896	0.07
	100000	0.0407	0.03896	0.03896	0.07
	100	1.283	0.6103	0.239	8.49
	200	1.258	0.6096	0.236	8.56
	400	1.190	0.6008	0.241	8.99
	600	1.134	0.5808	0.211	9.06
	800	1.042	0.5508	0.211	9.37
	1000	0.953	0.5132	0.194	9.54
	2000	0.567	0.3127	0.110	10.31
	4000	0.2275	0.1744	0.0329	11.66
	6000	0.1213	0.1058	0.0395	12.33
	8000	0.0732	0.0717	0.0184	13.05
$\gamma^* 0$	10000	0.0572	0.0516	0.0123	14.95
	20000	0.0168	0.00346	0.00168	17.51
	40000	0.0048	0.00073	0.00032	23.44
	60000	0.0022	0.00032	0.00019	30.06
	100000	0.0003	0.00268	0.00019	37.08
	100	1.268	0.7189	0.169	15.3
	200	1.269	0.7164	0.168	15.4
	400	1.269	0.7080	0.168	15.5
	600	1.222	0.6806	0.154	16.9
	800	1.135	0.6166	0.105	16.2
$\gamma^* 0$	1000	1.039	0.6066	0.105	16.9
	2000	0.5703	0.4225	0.0425	17.7
	4000	0.2162	0.2347	0.0477	18.59
	6000	0.1171	0.1550	0.0593	18.8
	8000	0.0755	0.1093	0.0199	19.8
	10000	0.0471	0.0871	0.0425	20.5
	20000	0.0168	0.0210	0.0145	20.5
	40000	0.0048	0.0132	0.00139	20.1
	60000	0.0022	0.00619	0.000539	20.3
	100000	0.0003	0.00268	0.00019	40.4
$\gamma^* 0$	100	6.154	4.122	3.68	0.0006
	200	6.158	4.122	3.72	0.00041
	400	4.466	4.07	4.06	0.0435
	600	6.156	4.159	4.24	0.0377
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	4000	0.2275	0.1744	0.0329	11.66
	6000	0.1213	0.1058	0.0395	12.33
	8000	0.0732	0.0717	0.0184	13.05
	10000	0.0572	0.0516	0.0123	14.95
	20000	0.0168	0.00346	0.00168	17.51
	40000	0.0048	0.00073	0.00032	23.44
	60000	0.0022	0.00032	0.00019	30.06
$\gamma^* 0$	100000	0.0003	0.00268	0.00019	40.4
	100	1.268	0.7189	0.169	15.3
	200	1.269	0.7164	0.168	15.4
	400	1.269	0.7080	0.168	15.5
	600	1.222	0.6806	0.154	16.9
	800	1.135	0.6166	0.105	16.2
	1000	1.039	0.6066	0.105	16.9
	20				

Table 2. Continued.

$\zeta$	$T = 1 h (3600 s)$			$h = 100 m$			$T = 2 h (7200 s)$			$h = 100 m$			$T = 3 h (10800 s)$			$h = 100 m$		
	$x$	$c_{\max}$	$D$	$\bar{c}$	$\lambda(s)$	$c_o$	$x$	$c_{\max}$	$D$	$\bar{c}$	$\lambda(s)$	$c_o$	$c_o$	$x$	$c_{\max}$	$D$	$\bar{c}$	$\lambda(s)$
	$10^{-5}$	$10^{-5}$	$10^{-5}$	$10^{-5}$	$10^{-3}$	$10^{-5}$		$10^{-5}$	$10^{-5}$	$10^{-5}$	$10^{-3}$	$10^{-3}$	$10^{-5}$		$10^{-5}$	$10^{-5}$	$10^{-5}$	$10^{-3}$
0.2	100	0.4083	0.2653	0.105	9.16	0.00022	100	0.3918	0.3717	0.0826	16.2	0.00022	0.00022	100	0.4127	0.4176	0.06681	22.5
	200	0.4088	0.2668	0.103	9.34	0.00022	200	0.3918	0.3717	0.0821	16.3	0.00022	0.00022	200	0.4118	0.4155	0.06650	22.6
	400	0.2991	0.2079	0.100	9.74	0.00096	400	0.3792	0.3715	0.0811	16.5	0.00096	0.00096	400	0.4069	0.4162	0.06486	23.1
	600	0.2887	0.2022	0.098	9.94	0.00440	600	0.3682	0.3702	0.0789	16.9	0.00440	0.00440	600	0.4017	0.4140	0.06424	23.2
	800	0.2885	0.2024	0.098	9.95	0.00440	800	0.3593	0.3672	0.0783	16.9	0.00440	0.00440	800	0.3949	0.4072	0.06373	23.2
	1000	0.2885	0.2021	0.098	9.95	0.00440	1000	0.3496	0.3622	0.0755	17.2	0.00440	0.00440	1000	0.3859	0.4050	0.06204	23.5
	2000	0.2886	0.2015	0.098	9.95	0.00440	2000	0.3295	0.3122	0.0631	17.8	0.00440	0.00440	2000	0.3523	0.3509	0.05242	24.1
	4000	0.1685	0.1677	0.098	9.95	0.00440	4000	0.2685	0.2103	0.0603	18.8	0.00440	0.00440	4000	0.3751	0.3732	0.04283	24.2
	6000	0.1685	0.1677	0.098	9.95	0.00440	6000	0.2055	0.1482	0.0268	19.2	0.00440	0.00440	6000	0.3763	0.3751	0.04245	24.9
	8000	0.1685	0.1677	0.098	9.95	0.00440	8000	0.1729	0.1102	0.0191	20.2	0.00440	0.00440	8000	0.3728	0.3716	0.04167	25.9
	10000	0.1685	0.1677	0.098	9.95	0.00440	10000	0.1572	0.0858	0.0141	21.2	0.00440	0.00440	10000	0.3521	0.3516	0.04140	26.7
	20000	0.1685	0.1677	0.098	9.95	0.00440	20000	0.1212	0.0549	0.0079	22.2	0.00440	0.00440	20000	0.3470	0.3464	0.04073	27.4
	40000	0.1685	0.1677	0.098	9.95	0.00440	40000	0.0925	0.0347	0.0027	23.2	0.00440	0.00440	40000	0.3456	0.3450	0.04056	27.6
	60000	0.1685	0.1677	0.098	9.95	0.00440	60000	0.0623	0.0145	0.0007	24.2	0.00440	0.00440	60000	0.3432	0.3426	0.04036	28.4
	100000	0.1685	0.1677	0.098	9.95	0.00440	100000	0.0323	0.0047	0.0001	25.2	0.00440	0.00440	100000	0.3418	0.3412	0.04016	29.1
0.0	100	2.874	1.902	1.92	3.57	0.0005	100	2.830	3.958	1.97	7.25	0.0005	0.0005	100	2.830	5.226	1.726	10.9
	200	2.874	1.902	1.92	3.57	0.0005	200	2.831	3.957	1.97	7.29	0.0005	0.0005	200	2.831	5.241	1.715	11.0
	400	2.874	1.902	1.92	3.57	0.0005	400	2.833	4.024	1.98	7.49	0.0005	0.0005	400	2.832	5.269	1.709	11.1
	600	2.874	1.902	1.92	3.57	0.0005	600	2.835	4.066	1.89	7.76	0.0005	0.0005	600	2.830	5.298	1.673	11.4
	800	2.874	1.902	1.92	3.57	0.0005	800	2.830	4.108	1.91	7.76	0.0005	0.0005	800	2.836	5.326	1.662	11.4
	1000	2.874	1.902	1.92	3.57	0.0005	1000	2.834	4.149	1.92	7.76	0.0005	0.0005	1000	2.833	5.352	1.660	11.4
	2000	2.874	1.902	1.92	3.57	0.0005	2000	2.831	4.189	1.93	7.76	0.0005	0.0005	2000	2.839	5.419	1.711	11.4
	4000	2.792	1.912	1.91	3.57	0.0005	4000	2.891	4.275	1.88	7.92	0.0005	0.0005	4000	2.810	5.949	1.609	11.4
	6000	2.792	1.912	1.91	3.57	0.0005	6000	2.892	4.320	1.62	7.81	0.0005	0.0005	6000	2.747	5.421	1.590	11.4
	8000	2.792	1.912	1.91	3.57	0.0005	8000	2.894	4.362	1.46	7.82	0.0005	0.0005	8000	2.743	5.406	1.584	11.5
	10000	2.792	1.912	1.91	3.57	0.0005	10000	2.895	4.396	1.28	7.84	0.0005	0.0005	10000	2.747	5.347	1.547	11.5
	20000	2.792	1.912	1.91	3.57	0.0005	20000	2.896	4.429	1.12	7.84	0.0005	0.0005	20000	2.740	5.347	1.510	11.5
	40000	2.792	1.912	1.91	3.57	0.0005	40000	2.897	4.462	0.96	7.84	0.0005	0.0005	40000	2.733	5.347	1.483	11.5
	60000	2.792	1.912	1.91	3.57	0.0005	60000	2.898	4.495	0.80	7.84	0.0005	0.0005	60000	2.727	5.347	1.456	11.5
	100000	2.792	1.912	1.91	3.57	0.0005	100000	2.899	4.527	0.64	7.84	0.0005	0.0005	100000	2.721	5.347	1.429	11.5
-0.2	100	0.2991	0.2079	0.100	9.74	0.0005	100	0.3918	0.3717	0.0826	16.2	0.0005	0.0005	100	0.4127	0.4176	0.06681	22.5
	200	0.2991	0.2079	0.100	9.74	0.0005	200	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	200	0.4118	0.4162	0.06650	22.6
	400	0.2991	0.2079	0.100	9.74	0.0005	400	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	400	0.4109	0.4140	0.06424	23.0
	600	0.2991	0.2079	0.100	9.74	0.0005	600	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	600	0.4099	0.4072	0.06373	23.2
	800	0.2991	0.2079	0.100	9.74	0.0005	800	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	800	0.4059	0.4050	0.06204	23.5
	1000	0.2991	0.2079	0.100	9.74	0.0005	1000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	1000	0.4059	0.4050	0.06204	23.5
	2000	0.2991	0.2079	0.100	9.74	0.0005	2000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	2000	0.4059	0.4050	0.06204	23.5
	4000	0.2991	0.2079	0.100	9.74	0.0005	4000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	4000	0.4059	0.4050	0.06204	23.5
	6000	0.2991	0.2079	0.100	9.74	0.0005	6000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	6000	0.4059	0.4050	0.06204	23.5
	8000	0.2991	0.2079	0.100	9.74	0.0005	8000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	8000	0.4059	0.4050	0.06204	23.5
	10000	0.2991	0.2079	0.100	9.74	0.0005	10000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	10000	0.4059	0.4050	0.06204	23.5
	20000	0.2991	0.2079	0.100	9.74	0.0005	20000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	20000	0.4059	0.4050	0.06204	23.5
	40000	0.2991	0.2079	0.100	9.74	0.0005	40000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	40000	0.4059	0.4050	0.06204	23.5
	60000	0.2991	0.2079	0.100	9.74	0.0005	60000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	60000	0.4059	0.4050	0.06204	23.5
	100000	0.2991	0.2079	0.100	9.74	0.0005	100000	0.3918	0.3717	0.0821	16.3	0.0005	0.0005	100000	0.4059	0.4050	0.06204	23.5
0.0	100	0.4083	0.2653	0.105	9.16	0.00022	100	0.3918	0.3717	0.0826	16.2	0.00022	0.00022	100	0.4127	0.4176	0.06681	22.5
	200	0.4083	0.2653	0.105	9.16	0.00022	200	0.3918	0.3717	0.0826	16.2	0.00022	0.00022	200	0.4118	0.4162	0.06650	22.6
	400	0.4083	0.2653	0.105	9.16	0.00022	400	0.3918	0.3717	0.0826	16.2	0.00022	0.00022	400	0.4109	0.4140	0.06424	23.0
	600	0.4083	0.2653	0.105	9.16	0.00022	600	0.3918	0.3717	0.0826	16.2	0.00022	0.00022	600	0.4099	0.4072	0.06373	23.2
	800	0.4083	0.2653	0.105	9.16	0.00022	800	0.3918	0.3717	0.								

Table 2. Continued.

$T = 1 \text{ h (3600 s)}$		$h = 150 \text{ m}$		$T = 2 \text{ h (7200 s)}$		$h = 150 \text{ m}$		$T = 3 \text{ h (10800 s)}$		$h = 150 \text{ m}$	
$\zeta$	$x$	$c_{\max}$	$D$	$\bar{c}$	$\lambda(s)$	$c_o$	$\zeta$	$x$	$c_{\max}$	$D$	$\bar{c}$
	$\text{m}$	$10^{-5}$	$10^{-5}$	$10^{-5}$	$10^3$	$10^{-5}$		$\text{m}$	$10^{-5}$	$10^{-5}$	$10^3$
0.4	100	1.517	0.7965	0.829	3.46	100	1.541	2.205	1.12	7.12	20.8
	200	1.521	0.5172	0.621	3.50	200	1.540	2.205	1.12	7.17	10.8
	400	1.528	0.6056	0.621	3.60	400	1.539	2.256	1.12	7.27	10.9
	600	1.534	0.9026	0.621	3.60	600	1.540	2.288	1.12	7.27	10.9
	800	1.540	0.9486	0.621	3.61	800	1.540	2.322	1.12	7.49	1.011
	1000	1.540	0.895	0.621	3.61	1000	1.540	2.354	1.12	7.52	1.011
	2000	1.541	1.196	1.02	4.12	2000	1.542	2.055	1.12	7.78	1.011
	4000	1.541	1.441	1.25	4.12	4000	1.542	2.055	1.12	7.79	1.011
	6000	1.541	1.58	1.415	4.13	6000	1.542	2.054	1.12	7.81	1.011
	8000	1.542	1.76	4.16	4.15	8000	1.542	2.054	1.12	7.82	1.011
	10000	1.542	1.84	4.17	4.17	10000	1.542	2.054	1.12	7.85	1.011
	20000	1.542	0.7949	0.670	4.27	20000	1.542	2.054	1.12	7.86	1.011
	40000	1.542	0.3940	0.321	4.42	40000	1.542	2.054	1.12	7.87	1.011
	60000	1.542	0.2423	0.193	4.53	60000	1.542	2.054	1.12	7.88	1.011
	100000	1.542	0.1291	0.1244	4.71	100000	1.542	2.054	1.12	7.89	1.011
0.7	100	0.5434	0.3003	0.276	3.92	100	0.5523	0.7963	0.372	7.71	11.5
	200	0.5449	0.3080	0.279	3.98	200	0.5536	0.8021	0.372	7.76	11.5
	400	0.5476	0.3233	0.286	4.07	400	0.5540	0.8136	0.373	7.86	11.5
	600	0.5500	0.3387	0.292	4.17	600	0.5543	0.8249	0.373	7.97	11.5
	800	0.5524	0.3541	0.299	4.27	800	0.5543	0.8364	0.374	8.06	11.5
	1000	0.5528	0.3695	0.306	4.35	1000	0.5543	0.8476	0.368	8.38	11.5
	2000	0.5541	0.5203	0.402	4.66	2000	0.5543	0.8997	0.287	8.45	0.0067
	4000	0.5544	0.5164	0.392	4.74	4000	0.5543	0.8910	0.277	8.51	0.0067
	6000	0.5544	0.5203	0.522	4.81	6000	0.5543	0.8916	0.262	8.58	0.0067
	8000	0.5563	0.4805	0.4370	4.86	8000	0.5543	0.8916	0.252	8.65	0.0067
	10000	0.5563	0.4936	0.4370	4.86	10000	0.5543	0.8916	0.242	8.72	0.0067
	20000	0.5564	0.4766	0.5167	5.12	20000	0.5544	0.8916	0.232	8.79	0.0067
	40000	0.5564	0.4384	0.5300	5.51	40000	0.5544	0.8916	0.222	8.86	0.0067
	60000	0.5621	0.07908	0.0489	5.82	60000	0.5621	0.8916	0.212	8.93	0.0067
	100000	0.5621	0.04159	0.0229	6.30	100000	0.5621	0.8916	0.202	9.00	0.0067
0.2	100	0.1427	0.1007	0.0336	10.8	100	0.1442	0.1841	0.0377	17.6	24.1
	200	0.1428	0.1022	0.0441	10.8	200	0.1441	0.1848	0.0378	17.6	24.1
	400	0.1445	0.1051	0.0475	10.9	400	0.1441	0.1840	0.0372	18.0	24.1
	600	0.1450	0.1075	0.0475	11.3	600	0.1441	0.1840	0.0373	18.4	24.1
	800	0.1453	0.1110	0.0475	11.6	800	0.1441	0.1840	0.0373	18.4	24.1
	1000	0.1448	0.1130	0.0552	12.4	1000	0.1437	0.1874	0.0373	18.4	24.1
	2000	0.1436	0.1162	0.0517	13.7	2000	0.1397	0.1816	0.0369	18.7	24.1
	4000	0.1409	0.9713	0.0255	14.2	4000	0.1366	0.1804	0.0365	18.7	24.1
	6000	0.14728	0.7670	0.0177	15.2	6000	0.1397	0.1816	0.0366	19.2	24.1
	8000	0.1567	0.7745	0.0125	15.5	8000	0.1559	0.1816	0.0268	20.5	24.1
	10000	0.14934	0.4498	0.00915	17.7	10000	0.1629	0.1816	0.0262	21.5	24.1
	20000	0.14935	0.7453	0.0025	22.7	20000	0.1629	0.1816	0.0254	22.5	24.1
	40000	0.14935	0.3052	0.0046	24.6	40000	0.1629	0.1816	0.0254	23.5	24.1
	60000	0.14935	0.5984	0.0062	26.6	60000	0.1629	0.1816	0.0254	25.5	24.1
	100000	0.14935	0.1407	0.00107	27.3	100000	0.1629	0.1816	0.0254	26.8	24.1
0.1	100	0.5434	0.3003	0.276	3.92	100	0.5523	0.7963	0.372	7.71	11.5
	200	0.5449	0.3233	0.286	4.07	200	0.5536	0.8021	0.372	7.76	11.5
	400	0.5476	0.3387	0.292	4.17	400	0.5540	0.8136	0.373	7.86	11.5
	600	0.5500	0.3541	0.299	4.27	600	0.5543	0.8249	0.373	7.97	11.5
	800	0.5524	0.3695	0.306	4.35	800	0.5543	0.8364	0.374	8.06	11.5
	1000	0.5528	0.3695	0.306	4.35	1000	0.5543	0.8476	0.368	8.38	11.5
	2000	0.5541	0.3203	0.402	4.66	2000	0.5543	0.8997	0.287	8.45	0.0067
	4000	0.5544	0.5164	0.392	4.81	4000	0.5543	0.8910	0.277	8.51	0.0067
	6000	0.5544	0.5203	0.522	4.81	6000	0.5543	0.8916	0.262	8.58	0.0067
	8000	0.5563	0.4805	0.4370	4.86	8000	0.5543	0.8916	0.252	8.65	0.0067
	10000	0.5563	0.4936	0.4370	4.86	10000	0.5543	0.8916	0.242	8.72	0.0067
	20000	0.5564	0.4766	0.5167	5.12	20000	0.5544	0.8916	0.232	8.79	0.0067
	40000	0.5564	0.4384	0.5300	5.51	40000	0.5544	0.8916	0.222	8.86	0.0067
	60000	0.5621	0.07908	0.0489	5.82	60000	0.5621	0.8916	0.212	8.93	0.0067
	100000	0.5621	0.04159	0.0229	6.30	100000	0.5621	0.8916	0.202	9.00	0.0067
-0.2	100	0.1427	0.1007	0.0336	10.8	100	0.1442	0.1841	0.0377	17.6	24.1
	200	0.1428	0.1022	0.0441	10.8	200	0.1441	0.1848	0.0378	17.6	24.1
	400	0.1445	0.1051	0.0475	10.9	400	0.1441	0.1840	0.0372	18.0	24.1
	600	0.1450	0.1075	0.0475	11.3	600	0.1441	0.1840	0.0373	18.4	24.1
	800	0.1453	0.1110	0.0552	12.4	800	0.1387	0.1874	0.0374	18.4	24.1
	1000	0.1448	0.1130	0.0517	13.7	1000	0.1397	0.1894	0.0365	18.7	24.1
	2000	0.1409	0.9713	0.0255	14.2	2000	0.1366	0.1816	0.0366	19.2	24.1
	4000	0.14728	0.7670	0.0177	15.2	4000	0.1629	0.1816	0.0268	20.5	24.1
	6000	0.1567	0.7745	0.0125	15.5	6000	0.1629	0.1816	0.0262	21.5	24.1
	8000	0.14934	0.4498	0.00915	17.7	8000	0.1629	0.1816	0.0254	22.5	24.1
	10000	0.14935	0.7453	0.0025	22.7	10000	0.1629	0.1816	0.0254	23.5	24.1
0.2	100	0.1427	0.1007	0.0336	10.8	100	0.1442	0.1841	0.0377	17.6	24.1
	200	0.1428	0.1022	0.0441	10.8	200	0.1441	0.1848	0.0378	17.6	24.1
	400	0.1445	0.1051	0.0475	10.9	400	0.1441	0.1840	0.0372	18.0	24.1
	600	0.1450	0.1075	0.0475	11.3	600	0.1441	0.1840	0.0373	18.4	24.1
	800	0.1453	0.1110	0.0552	12.4	800	0.1387	0.1874	0.0374	18.4	24.1
	1000	0.1448	0.1130	0.0517	13.7	1000	0.1397	0.1894	0.0365	18.7	24.1
	2000	0.1409	0.9713	0.0255	14.2	2000	0.1366	0.1816	0.0366	19.2	24.1
	4000	0.14728	0.7670	0.0177	15.2	4000	0.1629	0.1816	0.0268	20.5	24.1
	6000	0.1567	0.7745	0.0125	15.5	6000	0.1629	0.1816	0.0262	21.5	24.1
	8000	0.14934	0.4498	0.00915	17.7	8000	0.1629	0.1816	0.0254	22.5	24.1
	10000	0.14935	0.7453	0.0025	22.7	10000	0.1629	0.1816	0.0254	23.5	24.1
0.4	100	0.1427	0.1007	0.0336	10.8	100	0.1442	0.1841	0.0377	17.6	24.1
	200	0.1428	0.1022	0.0441	10.8	200	0.1441				

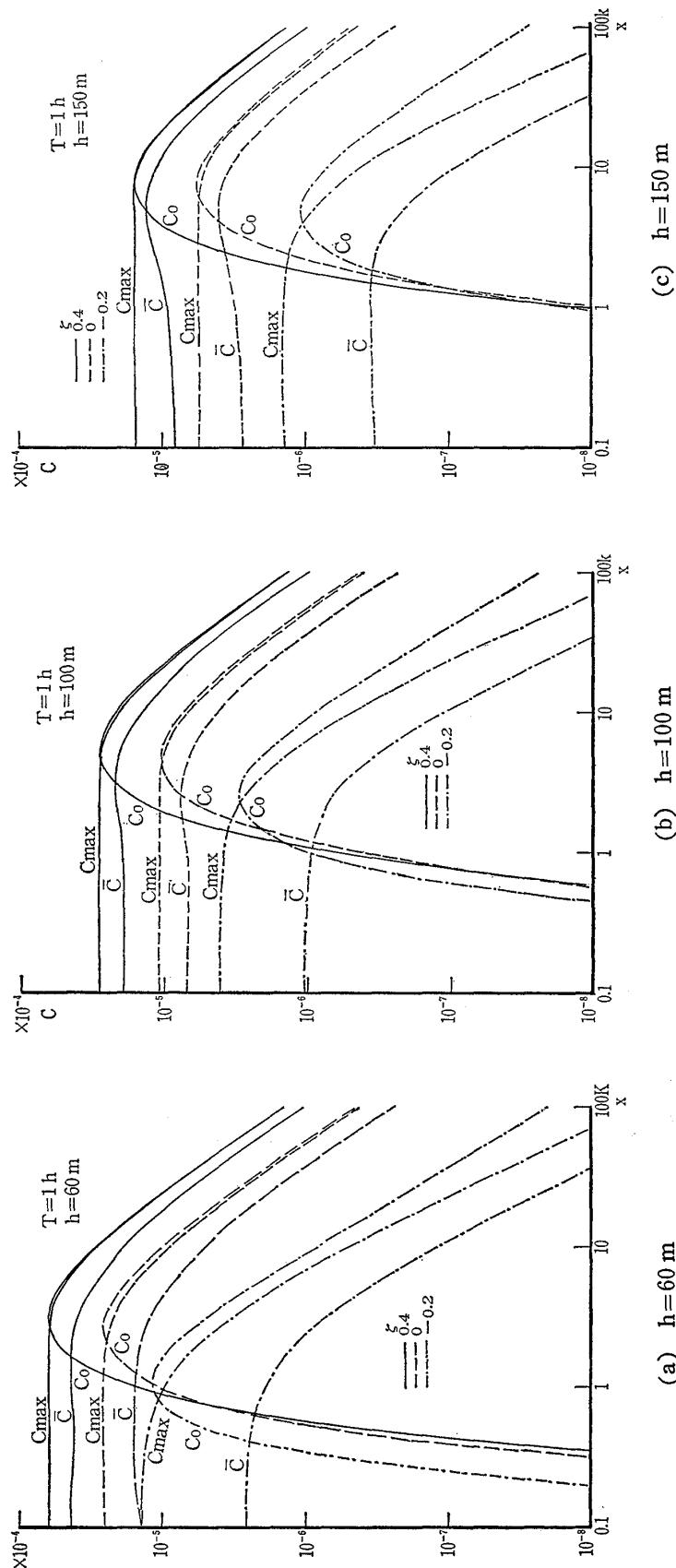


Fig. 5. Relations between  $C_{\max}$ ,  $D$ ,  $\bar{C}$ ,  $C_c$  and  $x$  for  $T=1\text{ h}$ .

or mean concentration  $\bar{C}$

$$\bar{C} = D/\lambda = \int_0^\infty C dt / \lambda$$

are essential. However, though  $\lambda$  is infinite theoretically, it is finite in practical sense, and there may be some ambiguities in determining the both ends of the interval. We assumed that the ends are the instants when the concentrations are  $10^{-4}$  of the maximum concentration.

We show the relations between  $C_{\max}$ ,  $\bar{C}$ ,  $\lambda$  and  $x$ , together with  $C_c$  which is the concentration of a continuous plume. (Table 2).

Results of the cases  $T=1 h$ ,  $\zeta=0$ :  $h=60, 100$  and  $150 m$  are shown in Fig. 5 a, b and c.

As a representative case, time changes of concentration for  $T=1$ ,  $2$  and  $3 h$  are shown in Fig. 6. When  $T$ 's become longer, the curves do not change in the main part and only extend themselves their latter parts.

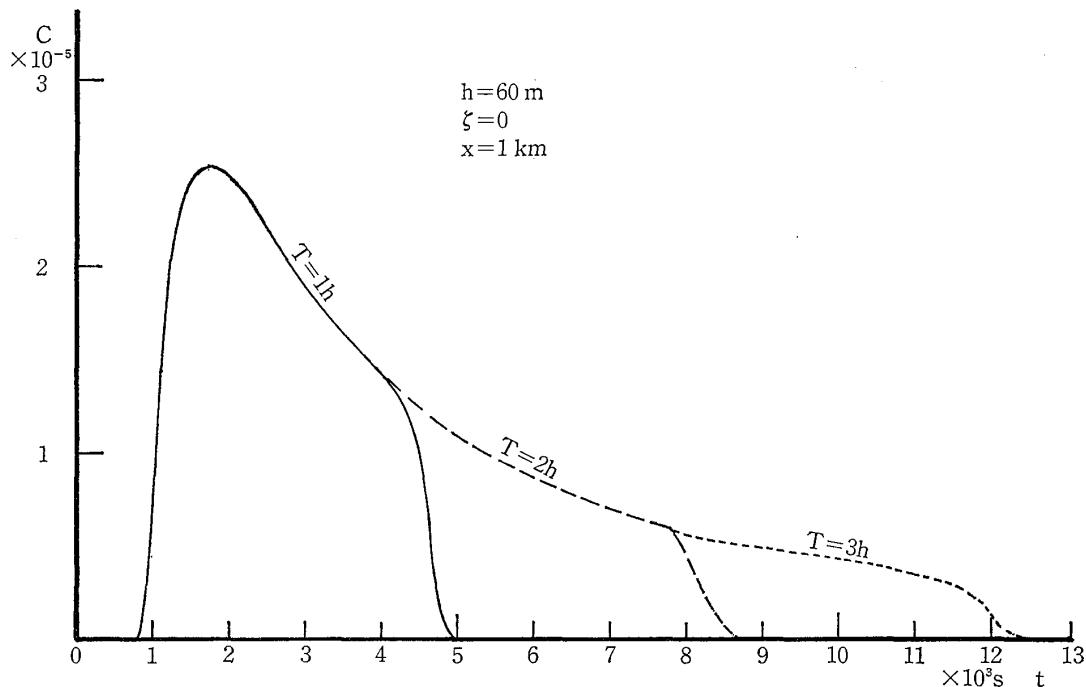


Fig. 6. Time changes of concentration for  $T=1, 2$  and  $3 h$ .

2)  $\theta=175^\circ$ : The ground level concentrations were calculated in the cases of  $h=60 m$ ,  $T=1 h$ ,  $\zeta=0$ ,  $u_1=u_2=1 m/s$ ;  $x=100$ ,  $y=0$  ( $l_1=-99.62$ ,  $l_2=8.716$ )  $m$  and  $x=1000$ ,  $y=0$  ( $l_1=-996.2$ ,  $l_2=87.16$ )  $m$ .

The results are shown in Fig. 7. The graphs differ considerably with those in the case  $\theta=180^\circ$ . The values of  $\bar{C}$  are shown in Table 3.

3)  $\theta=90^\circ$ : The calculation was carried out in the cases  $h=60 m$ ,  $T=1 h$ ,  $\zeta=0$ ,  $u_1=u_2=1 m/s$ :  $x=100$ ,  $y=100$  ( $l_1=100$ ,  $l_2=100$ );  $x=100$ ,

$y=1000$  ( $l_1=1000$ ,  $l_2=100$ ) ;  $x=1000$ ,  $y=100$  ( $l_1=100$ ,  $l_2=1000$ ) and  $x=1000$ ,  $y=1000$  ( $l_1=1000$ ,  $l_2=1000$ ) m.

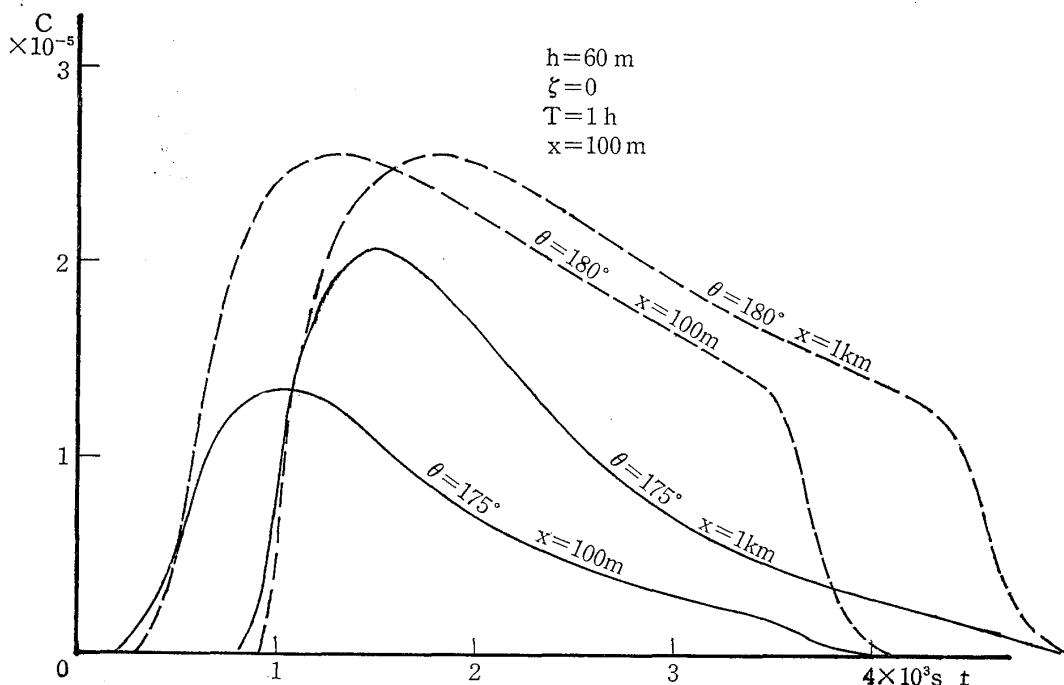


Fig. 7. Time changes of concentration for  $\theta=175^\circ$  and  $180^\circ$  in the case of  $h=60$  m,  $\zeta=0$ ,  $T=1$  h and  $x=100$  m.

Table 3. Relations between  $C_{\max}$ , D,  $\bar{C}$ ,  $\lambda$  and  $\theta^\circ$ .

$T = 1$  h (3600 s),  $h = 60$  m,  $\zeta = 0$

$\theta$ ( $^\circ$ )	x (m)	y (m)	$C_{\max}$	D (ch)	$\bar{C}$	$\lambda$ (s)
180	100	0	2.55(-5)	1.47(-5)	1.57(-5)	3700
175	100	0	1.34(-5)	6.36(-6)	6.18(-6)	3700
	1000	0	2.07(-5)	9.94(-6)	8.73(-6)	4100
90	100	100	1.27(-12)	1.65(-12)	4.94(-11)	130
	100	1000	1.20(-12)	4.69(-5)	5.76(-6)	260
	1000	100	1.00(-5)	3.75(-4)	3.99(-6)	330
	1000	1000	1.16(-5)	4.42(-4)	4.65(-6)	350

The results are shown in Fig. 8 and 9. The exposed intervals become very short compared with above two cases and the values of  $\bar{C}$  become considerably small (Table 3).

### Consideration

- 1) The value of  $u_1$  affects the concentration and the length of the plume in the first stage, and that of  $u_2$  affects the duration of the exposed interval and on the value of dosage, but does not affect  $\bar{C}$ .

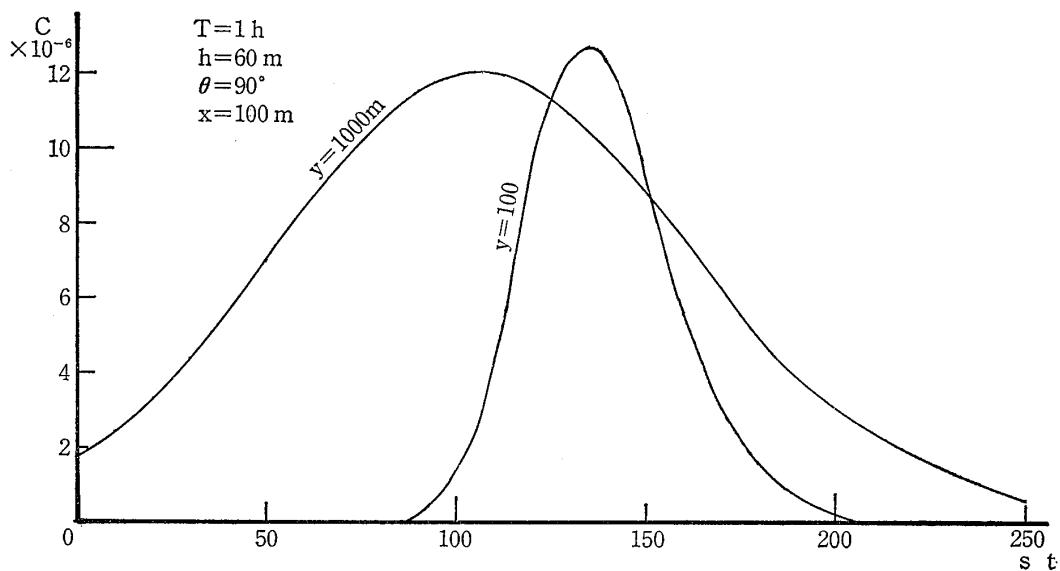


Fig. 8. Time changes of concentration in the cases of  $\theta = 90^\circ$ ,  $h = 60 \text{ m}$ ,  $\zeta = 0$ ,  $T = 1 \text{ h}$ ,  $x = 100 \text{ m}$ ,  $y = 100 \text{ m}$  and  $1000 \text{ m}$ .

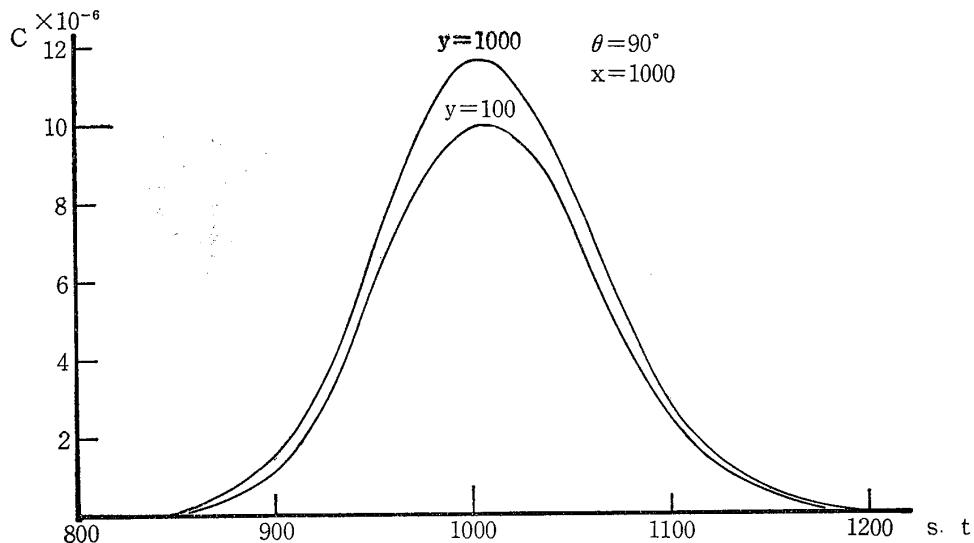


Fig. 9. Time changes of concentration in the cases of  $\theta = 90^\circ$ ,  $h = 60 \text{ m}$ ,  $\zeta = 0$ ,  $T = 1 \text{ h}$ ,  $x = 1000 \text{ m}$ ,  $y = 100$  and  $1000 \text{ m}$ .

- 2) In the case when  $\theta$  is nearly  $180^\circ$ , the concentrations of continuous source  $C_c$  are very low in the region near the source, but those resulted in the second stage are considerably high.
- 3) The values of  $\bar{C}$  in the case of  $175^\circ$  are considerably less than those in the case of  $180^\circ$ . Only the difference of  $5^\circ$  affects remarkably.
- 4) When  $\theta =$  is nearly  $90^\circ$ , the exposed intervals become very short, and the concentrations become much lower.

### Literature

- (1) Sakagami, J.: 1954, On the Turbulent Diffusion in the Atmosphere, Natural Science Rep., Ochanomizu Univ., 5 (1), pp. 79-91.  
Sakagami, J.: 1960, On the Relations between the Diffusion Parameters and Meteorological Conditions, ditto, 11 (1), pp. 7-27.